



---

# Detecting Circuit Breaker Status Errors in Substations

*Part II of Final Project Report*

**Power Systems Engineering Research Center**

*A National Science Foundation  
Industry/University Cooperative Research Center  
since 1996*





**Power Systems Engineering Research Center**

**Detecting Circuit Breaker Status Errors  
in Substations**

**Final Project Report**

**Part II**

**Report Authors**

**Jun Zhu  
Ali Abur  
Texas A&M University**

**PSERC Publication 05-57**

**October 2005**

## **Information about this project**

For information about this project contact:

Ali Abur, Ph.D.  
Texas A&M University  
Department of Electrical Engineering  
College Station, TX 77843-3128  
Phone: 979-845-1493  
FAX: 979-845-9887  
Email: abur@ee.tamu.edu

## **Power Systems Engineering Research Center**

This is a project report from the Power Systems Engineering Research Center (PSERC). PSERC is a multi-university Center conducting research on challenges facing a restructuring electric power industry and educating the next generation of power engineers. More information about PSERC can be found at the Center's website: <http://www.pserc.org>.

For additional information, contact:

Power Systems Engineering Research Center  
Cornell University  
428 Phillips Hall  
Ithaca, New York 14853  
Phone: 607-255-5601  
Fax: 607-255-8871

## **Notice Concerning Copyright Material**

PSERC members are given permission to copy without fee all or part of this publication for internal use if appropriate attribution is given to this document as the source material. This report is available for downloading from the PSERC website.

## **Acknowledgements**

The Power Systems Engineering Research Center sponsored the research project titled “Enhanced Reliability of Power System Operation Using Advanced Algorithms and IEDs for On-Line Monitoring” (PSERC project T-17). This is Part II of the final report on that project.

We express our appreciation for the support provided by PSERC’s industrial members and by the National Science Foundation under grant NSF EEC-0002917 received under the Industry / University Cooperative Research Center program.

The authors thank PSERC members for their technical advice on the project, especially M. Ingram (TVA), D. Sevcik (CenterPoint Energy), M. Subramanian (ABB), D. Krummen (AEP), A. Mander (Tri-State G&T Association), L. Priez (Entergy), J. Bell (TXU), and P. Kaptain (WAPA) who are industry advisors for the project. The authors also acknowledge Professors A. P. Sakis Meliopoulos of Georgia Tech and Rahmat Shoureshi of Colorado School of Mines who provided technical advice to this work. Professor Kezunovic is the project leader.

## Executive Summary

State estimation is a crucial function for reliable and secure operation of power systems, and for efficient power market operations. Successful use of state estimators requires minimization of possible errors that would lead to inaccurate estimates of the power system condition and, as a result, to inaccurate information for power system operators. Circuit breaker status errors can produce such errors because the state estimator would be estimating the system condition for a power system whose topology is not the same as the actual system topology.

Recently a new method, based on a reduced system model and Lagrange multipliers, was proposed for topology error analysis. In this method, the size of a detailed substation model is reduced by applying Kirchhoff's law and by implicitly considering topological constraints. This model reduction is achieved without losing any capability to detect and identify topology errors. The method has an important advantage over existing topological analysis techniques in that the user does not have to specify the suspect substation ahead of time because all substations can be modeled by using a small number of extra state variables.

Only simulation results for one substation have been shown in the literature for this new method. Extensive testing on practical test systems has not yet been reported. This project investigates the method and its implementation to evaluate its possible performance for practical, multi-substation power systems. The method is implemented and tested on the IEEE 14, 30 and 57 bus test systems using simulated data and topology error scenarios.

The main two purported advantages of the implemented method are its ability to detect status errors associated with substation breakers without significantly increasing the size of the network model, and to differentiate between analog measurement errors and breaker status errors. Both advantages were validated using simulated cases. As a result, the method is recommended as a new feature for state estimation software.

## Table of Contents

1. Introduction.....	1
2. Method of Implicit Model.....	2
2.1 Building the Tree .....	2
2.2 Computing Lagrange Multipliers.....	3
2.3 Normalization of Lagrange Multipliers .....	6
3. Topology Error Identification Algorithm .....	7
3.1 Overall Process .....	7
3.2 Flow Chart .....	7
4. Simulation Results .....	10
4.1 Topology or Measurement Error .....	10
4.2 Simultaneously Occurring Measurement and Topology Errors .....	12
4.3 Computation Time .....	13
5. Program Data Structure.....	14
5.1 Input Data Files.....	14
5.1.1 topoanainput.dat .....	14
5.1.2 topomeasure.dat.....	15
5.1.3 vinput.dat.....	17
5.2 Output Data Files.....	17
6. Conclusions and Future Work .....	20
REFERENCES .....	20
APPENDIX 1. Matlab Code of the Method .....	22
APPENDIX 2. Input Data Files Generating Program .....	35

## Table of Figures

<b>Figure 1.1</b> Substation graph .....	2
<b>Figure 1.2</b> Proper tree.....	2
<b>Figure 3.1</b> Flow chart.....	8
<b>Figure 4.1</b> 4-CB substation model .....	12
<b>Figure 8.1</b> One-line substation model .....	35
<b>Figure 8.2</b> Two-line substation model .....	36
<b>Figure 8.3</b> Three-line substation model .....	36
<b>Figure 8.4</b> Four-line substation model .....	37
<b>Figure 8.5</b> Five-line substation model.....	38
<b>Figure 8.6</b> Six-line substation model .....	39
<b>Figure 8.7</b> Seven-line substation model.....	40

## Table of Tables

<b>Table 4.1</b> Simulated Topology and Measurement Errors .....	10
<b>Table 4.2</b> Results of Error Identification - 14-bus System.....	11
<b>Table 4.3</b> Results of Error Identification - 30-bus System.....	11
<b>Table 4.4</b> Results of Error Identification - 57-bus System.....	11
<b>Table 4.5</b> Multiple Error Identification Results - 14-bus System .....	13
<b>Table 4.6</b> Comparison of Computation Time.....	13

## 1. Introduction

---

Topology error analysis is one of the important functions which assure the validity of the data used in power system state estimation. Normally, topology of the power system refers to the topology between and within the substations in the system, that is, the status of the circuit breakers in the substation. Traditional state estimation is carried out assuming that the status of the circuit breakers are all known, then all the inconsistencies resulted will be blamed on the analog measurements. However, the wrong status of a circuit breaker, which will typically lead to the outage of a line, will cause much more severe errors in the state estimation results.

Considering computational limits, detailed substation models including circuit breakers are only involved for small sub networks surrounding the suspect area in traditional topology analysis method. As a result, the suspected area has to be determined a priori state estimation by other techniques [1,2,3,4,5].

Recently, a new method based on reduced system model and Lagrange multipliers is proposed [6]. In this method, the size of the detailed substation model is reduced by applying Kirchhoff's law and implicitly considering the topological constraints. This is achieved without losing any capability to detect and identify topology errors. However, only the simulation results within one substation are shown in that paper.

The objective of this report is to testify the validity of the topology analysis method stated above in a realistic power system. The report is organized as follows. Section II briefly presents the theory and formulation of the method. Section III gives the flow chart of the method. The simulation results are given in section IV. The input and output data structure is introduced in section V. Section VI concludes the report, followed by the Appendix.

## 2. Method of Implicit Model

---

In this section, a brief presentation of the implicit model method will be given. It is composed of three parts: (1) how to build the tree of the substation, (2) how to compute the Lagrange multipliers, and (3) how to normalize them.

### 2.1 Building the Tree

In order to simplify the detailed substation model, a tree is built. This way, any of the power flows and voltage drops in the substation graph could be expressed in terms of the power flows of the tree branches and the voltage drops across the tree links, respectively. Moreover, a proper tree is a useful structure to determine the constraints of the circuit breakers.

The proper tree is defined as follows.

- 1) Exclude all nonzero impedance branches.
- 2) Include as many closed CBs as possible.
- 3) Select, for every electrical bus, a nonzero injection node that will be termed the base node. Include the respective injection branch in the tree. An electrical bus exclusively connected to nonzero impedance branches constitutes a special case which is handled by adding a virtual null-injection branch to any of its elemental buses. This extra branch, also included in the tree, irresponsible for the null-injection constraints conventionally used by SEs.
- 4) If the case arises, complete the tree with CBs the status of which is unknown.
- 5) Exclude as many open CBs as possible.

Figure 1.2 shows the proper tree of the substation of Figure 1.1.

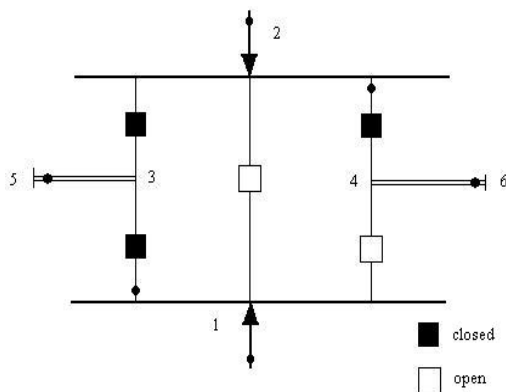


Figure 1.1 Substation graph

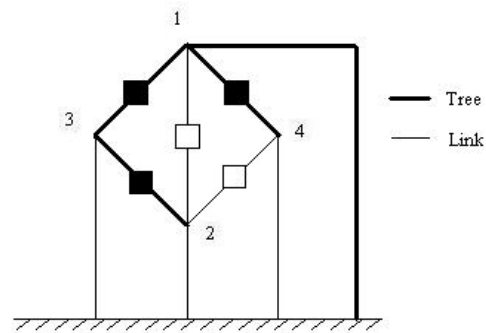


Figure 1.2 Proper tree

This is the rule of tree building of a substation. For a whole system, the non-zero impedance branches will be connected to each other and there will be a common reference picked for all the injections.

## 2.2 Computing Lagrange Multipliers

From the proper tree built, the proper model can be written as follows:

$$z = h(x_I, x_{CB}) + e \quad (2.1)$$

$$c(x_I, x_{CB}) = 0 \quad (2.2)$$

$$x_{CB} = 0 \quad (2.3)$$

where the following notation is adopted:

$x_I$  : Component of the state vector containing:

Voltage magnitude and phase angle of all base nodes (each one representing an electrical node).

Voltage magnitude and phase angle across unknown and open CBs belonging to the proper tree.

Power flows through links of the proper tree corresponding to injections, as well as unknown and closed CBs.

$x_{CB}$  : Component of the state vector comprising.

Voltage magnitude and phase angle across closed CBs included in the proper tree.

Power flows through open CBs excluded from the proper tree.

For example, for substation shown in Fig. 1:

$$x_I = [\theta_1, p_2]^T$$

$$x_{CB} = [\theta_{23}, \theta_{23}, \theta_{14}, p_{12}, p_{24}]^T$$

For equation (2.1), the measurement vector  $z$  is expressed as a sum of  $h(x_I, x_{CB})$  and the vector  $e$ .  $h(x_I, x_{CB})$  is the nonlinear function of both  $x_I$  and  $x_{CB}$ , which are the state vectors, and  $e$  is the vector of measurement errors. Equation (2.2) gives the equality constraints contributed by zero-injections on buses. Topology errors are normally assumed to be zero by state estimator. Therefore, for error free operation, the equality constraints of CBs can be written as shown in equation (2.3). For closed CBs in the tree and open CBs in the co-tree, the constraint equations can be written as  $\theta_{ab} = 0$  and  $p_{cd} = 0$ , respectively. As mentioned in the previous section, a proper tree will make equation (2.3) as simple as possible.

The weighted least square state estimation problem in the presence of network topology errors and equality constraints can then be formulated as the following optimization problem:

$$\begin{aligned} \text{Minimize} \quad & J(x_I, x_{CB}) = \frac{1}{2} r^t W r \\ \text{Subject to} \quad & c(x_I, x_{CB}) = 0 \\ & x_{CB} = 0 \end{aligned} \quad (2.4)$$

where:

$r = z - h(x_I, x_{CB})$  is the measurement residual vector,

$W$  is the diagonal matrix whose inverse is the measurement error covariance matrix,  $\text{cov}(e)$ .

Applying the method of Lagrange multipliers, the Lagrangian of proper model becomes

$$L = \frac{1}{2} r^t W r - \mu^t c(x_I, x_{CB}) - \lambda^t x_{CB} \quad (2.5)$$

and the following first-order optimality conditions can be written as

$$\frac{\partial L}{\partial x_I} = H_I^t W r + C_I^t \mu = 0 \quad (2.6)$$

$$\frac{\partial L}{\partial x_{CB}} = H_{CB}^t W r + C_{CB}^t \mu + \lambda = 0 \quad (2.7)$$

$$\frac{\partial L}{\partial \mu} = c(x_I, x_{CB}) = 0 \quad (2.8)$$

$$\frac{\partial L}{\partial \lambda} = x_{CB} = 0 \quad (2.9)$$

where:

$H_I$ ,  $H_{CB}$  and  $C_I$ ,  $C_{CB}$  are the gradients of  $H$  and  $C$  with respect to  $x_I$  and  $x_{CB}$ , respectively.

$\mu$  and  $\lambda$  are the Lagrange multipliers for the equality constraints (2.1) and (2.2).

Equation (2.7) allows the multiplier  $\lambda$  to be expressed in terms of  $r$  and  $\mu$ .

$$\lambda = T \begin{bmatrix} r \\ \mu \end{bmatrix} \quad (2.10)$$

where

$$T = - \begin{bmatrix} WH_{CB} \\ C_{CB} \end{bmatrix}^t \quad (2.11)$$

is the topological sensitivity matrix.

Equation (2.3) allows the substitution of  $x_{CB}$  in equations (2.6)-(2.8). Denoting  $h(x_I, 0)$  and  $c(x_I, 0)$  by  $h_0(x_I)$ ,  $c_0(x_I)$  respectively, the proper model becomes the implicit model

$$z = h_0(x_I) + e \quad (2.12)$$

$$c_0(x_I) = 0 \quad (2.13)$$

Note that equation (2.12) and (2.13) provides exactly the same results as the original model without explicitly handling topological constraints.

Substituting the first order Taylor approximations for  $h_0(x_I)$  and  $c_0(x_I)$ , the following linear equations will be obtained:

$$H_I \cdot \Delta x_I + r = \Delta z \quad (2.14)$$

$$C_I \cdot \Delta x_I = -c_0(x_{I0}) \quad (2.15)$$

where:

$$\Delta x_I = x_I - x_{I0},$$

$$\Delta z = z - h_0(x_{I0}).$$

$x_{I0}$  being the initial guess for the system state vector

Using (2.6), (2.14), and (2.15), the following equation will be obtained:

$$\begin{bmatrix} 0 & H_I^t W & C_I^t \\ H_I & I & 0 \\ C_I & 0 & 0 \end{bmatrix} \bullet \begin{bmatrix} \Delta x_I \\ r \\ \mu \end{bmatrix} = \begin{bmatrix} 0 \\ \Delta z \\ -c_0(x_{I0}) \end{bmatrix} \quad (2.16)$$

Equation (2.16) is similar to the equation used in conventional WLS state estimation except for the fact that state variables are not exactly the same. The measurement residuals  $r$  and the Lagrange multipliers for the zero injections  $\mu$  can be obtained first by iteratively solving (2.16). Once the state estimation algorithm successfully converges, (2.10) can be used to recover the Lagrange multiplier vector associated with the topology errors.

### 2.3 Normalization of Lagrange Multipliers

To identify topology errors, the validity of the constraints (8) has to be tested. This can be done by checking the Lagrange multiplier vector  $\lambda$  associated with the topology error vector  $x_{CB}$ . However, it has to be normalized by its covariance matrix  $\text{cov}(\lambda)$  before testing of its significance.

Letting  $u = [r \quad \mu]^T$  and using (2.10):

$$\Lambda = \text{cov}(\lambda) = T \cdot \text{cov}(u) \cdot T^t \quad (2.17)$$

The covariance of  $u$ ,  $\text{cov}(u)$  can be calculated by first expressing  $r$  and  $\mu$  in terms of the measurement mismatch. To do that, let the inverse of the coefficient matrix in (2.16) be given in partitioned form as follows:

$$\begin{bmatrix} 0 & H_I^t W & C_I^t \\ H_I & I & 0 \\ C_I & 0 & 0 \end{bmatrix}^{-1} = \begin{bmatrix} E_1 & E_2 & E_3 \\ E_4 & E_5 & E_6 \\ E_7 & E_8 & E_9 \end{bmatrix} \quad (2.18)$$

Noting that  $c_0(x) = 0$  at the solution, (2.16) will yield the following expressions for  $r$  and  $\mu$ :

$$r = E_5 \cdot \Delta z \quad (2.19)$$

$$\mu = E_8 \cdot \Delta z \quad (2.20)$$

Let  $\Psi = [E_5 \quad E_8]^T$ , then:

$$u = \Psi \cdot \Delta z \quad (2.21)$$

$$\text{cov}(u) = \Psi^{-1} \cdot W \cdot \Psi \quad (2.22)$$

The Lagrange multipliers for the topology errors can then be normalized using the diagonal elements of the covariance matrix  $\Lambda$  defined in (2.19):

$$\lambda_i^N = \frac{\lambda_i}{\sqrt{\Lambda(i,i)}} \quad (2.23)$$

for all  $i = 1 \dots k$ , where  $k$  is the total number of CBs whose errors are to be identified.

### 3. Topology Error Identification Algorithm

---

#### 3.1 Overall Process

Using the method presented in section 2, a topology error detection and identification can be carried out as described below:

##### Step 1. Topology Processing

First a proper tree is selected for each substation. Based on the tree, the state variables are categorized into two groups,  $x_I$  and  $x_{CB}$ . Then the Jacobian matrix  $H$  is partitioned into two sub matrices,  $H_I$  and  $H_{CB}$ . This step constitutes the backbone of the algorithm.

##### Step 2. State Estimation

Except for the size of the state and measurement vectors, this procedure is essentially identical to traditional state estimation carried out by existing methods. The solution will yield both the measurement residual vector  $r$  and the Lagrange multiplier vector  $\mu$  of zero injections if they are treated as equality constraints in the state estimation formulation.

##### Step 3. Normalization of $r^N$ and $\lambda^N$

Compute the normalized residuals  $r^N$  for the measurements and the normalized Lagrange multipliers  $\lambda^N$  for the topology errors using the procedure outlined in section II above.

##### Step 4. Bad Data and Topology Error Identification

Choose the larger one between the largest normalized residual and the largest normalized Lagrange multiplier.

- If the chosen value is below the identification threshold, then no bad data or parameter error will be suspected. A statistically reasonable threshold to use is 3.0, which is the one used in all simulations presented in the next section.
- Else, the measurement or the parameter corresponding to the chosen largest value will be identified as the source of error in estimation.

Note that the bad data and topology error analysis are conducted simultaneously. That means this algorithm can identify the topology error even with the interference of the bad data, and clear them one by one. Furthermore, only a small subset of substations should be suspicious in practice, as topology errors are not frequent. In this algorithm, the detailed substation data of those suspicious substations can be combined with the normal bus data. Since the entire substation blocks are decoupled in T matrix, the computational burden will be largely decreased this way.

#### 3.2 Flow Chart

The flow chart of the algorithm is shown below.

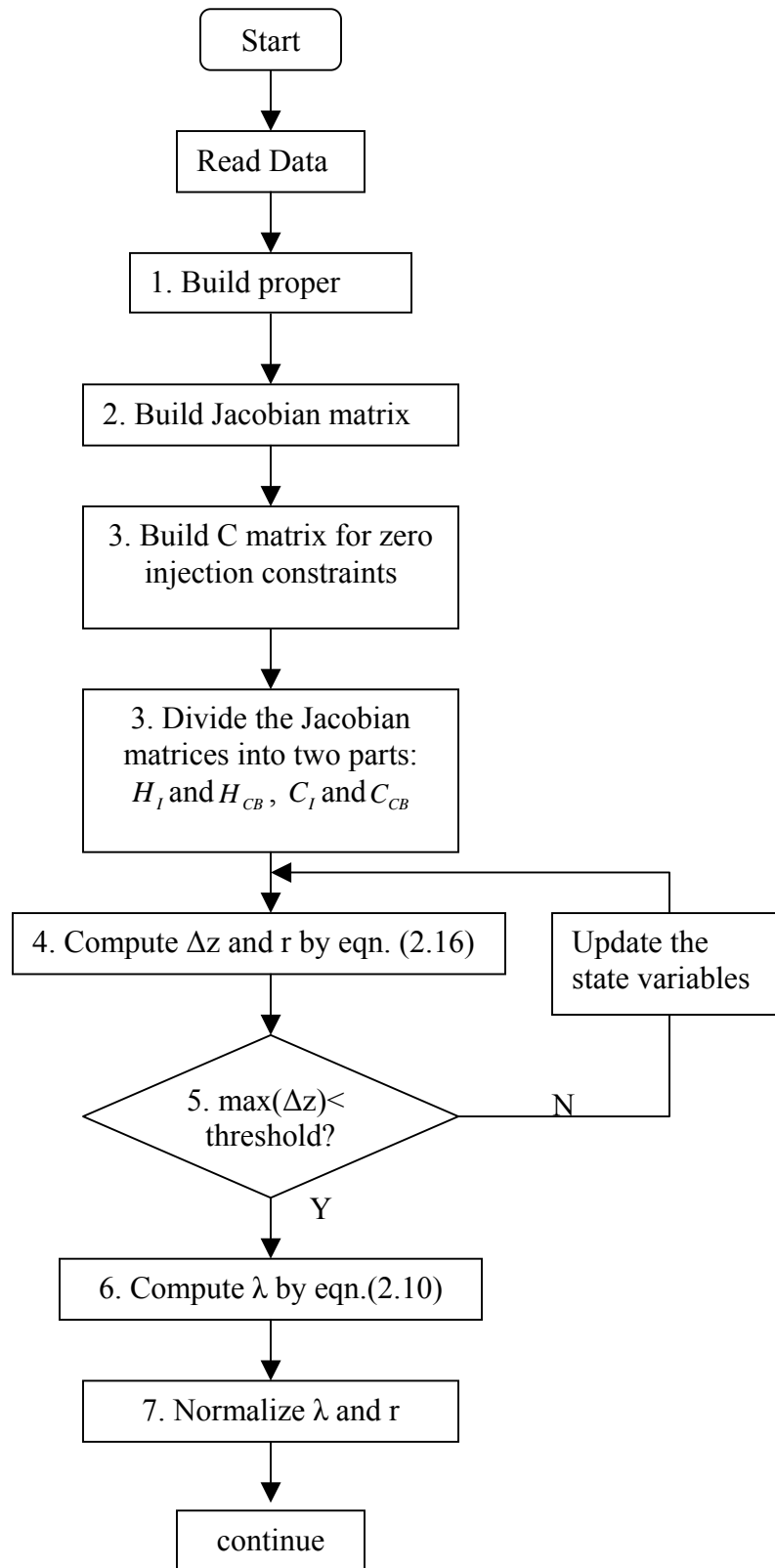


Figure 3.1 Flow Chart

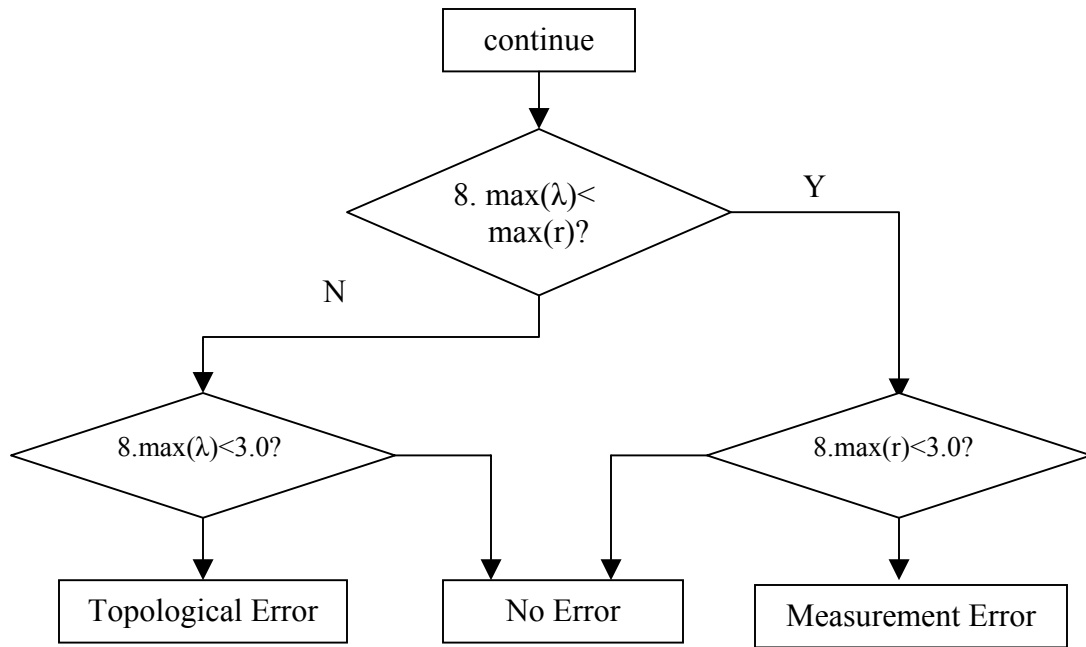


Figure 3.1 Flow Chart (continued)

## 4. Simulation Results

---

The above described topology error identification procedure is implemented and tested on IEEE 14, 30 and 57 bus test systems. Different cases are simulated where errors are introduced in the circuit breakers and analog measurements. Both single errors and simultaneously occurring errors in analog measurements and circuit breaker status are simulated.

### 4.1 Topology or Measurement Error

This case presents single errors in circuit breaker status or analog measurement. The method is shown to differentiate between these different types of errors and to correctly identify the error. The simulated errors for the three test systems are listed in Table 1, where the tests A and B are carried out as follows:

Test A: The status of the circuit breaker listed in Table 1 is wrong; all analog measurements are error free. There is a disconnected line as a result of that circuit breaker's operation.

Test B: No topology errors are introduced; all measurements are error free except for the listed flows in Table 4.1. Tables 4.2-4.4 show the sorted normalized residuals  $r_N$  and normalized Lagrange multipliers  $\lambda_N$ , obtained during the tests of Table 1, only the 5 largest ones are listed.

Table 4.1 Simulated Topology and Measurement Errors

Test System	Wrong status CB & Outaged Line/Meas.		
	Test A		Test B
14-bus	$CB_{34-32}$	Line 5-6	$P_{34-32}$
30-bus	$CB_{74-68}$	Line 10-22	$P_{74-68}$
57-bus	$CB_{80-78}$	Line 4-6	$P_{80-78}$

Table 4.2 Results of Error Identification - 14-bus System

Test A		Test B	
<i>Measurement/Topology</i>	<i>Normalized residual / <math>\lambda^N</math></i>	<i>Measurement/Topology</i>	<i>Normalized residual / <math>\lambda^N</math></i>
$CB_{34-32}$	1008.06	$P_{34-32}$	84.79
$CB_{36-32}$	1008.06	$CB_{33-34}$	40.04
$CB_{5-33}$	944.46	$CB_{36-32}$	26.60
$CB_{5-35}$	944.46	$CB_{34-32}$	26.60
$CB_{33-34}$	942.43	$CB_{35-36}$	22.64

Table 4.3 Results of Error Identification - 30-bus System

Test A		Test B	
<i>Measurement/Topology</i>	<i>Normalized residual / <math>\lambda^N</math></i>	<i>Measurement/Topology</i>	<i>Normalized residual / <math>\lambda^N</math></i>
$CB_{74-68}$	212.30	$P_{74-68}$	97.18
$CB_{70-68}$	199.09	$CB_{74-68}$	38.37
$CB_{10-71}$	160.95	$CB_{73-74}$	38.12
$CB_{105-104}$	157.04	$CB_{36-34}$	28.00
$CB_{106-104}$	157.04	$CB_{33-31}$	22.59

Table 4.4 Results of Error Identification - 57-bus System

Test A		Test B	
<i>Measurement/Topology</i>	<i>Normalized residual / <math>\lambda^N</math></i>	<i>Measurement/Topology</i>	<i>Normalized residual / <math>\lambda^N</math></i>
$CB_{80-78}$	371.63	$P_{80-78}$	96.40
$CB_{82-78}$	371.63	$P_{1228-124}$	39.08
$CB_{81-82}$	282.65	$CB_{80-78}$	37.87
$CB_{76-75}$	212.03	$CB_{82-78}$	37.87
$CB_{77-75}$	212.03	$CB_{79-80}$	36.93

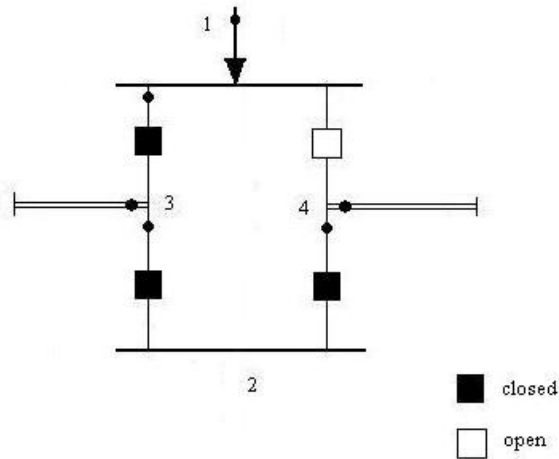


Figure 4.1 4-CB substation model

Note that in Tables 4.2 and 4.4, there are two equal largest normalized Lagrange multipliers. That is because these two circuit breakers form a critical pair like the circuit breakers 2-3 and 2-4 shown in Figure 4.1. By changing the status from closed to open, either CB 2-3 or 2-4 can disconnect the line at bus 4. Such errors can be detected but not identified. By the simulation results shown above, single circuit breaker status error or single measurement error can be detected and identified based on the specific topology of that substation.

## 4.2 Simultaneously Occurring Measurement and Topology Errors

This case shows the identification of multiple errors occurring simultaneously in the 14-bus system. Errors are simulated for the status of CB 31-26, and for the power flow measurement p28-26 in substation 4. Note that the two errors are highly correlated. Two tests are carried out as follows:

Test A: The bias in the measurement is 50% of the true value.

Test B: The bias in the measurement is 100% of the true value.

Table 4.5 shows the sorted normalized residuals  $r_N$  and normalized Lagrange multipliers  $\lambda_N$  of the two tests, only the 5 largest ones are listed.

When there are multiple errors in the CB status as well as the measurement, the program can identify the most influential error among all the errors as shown in Table 4.5. Similar to the case of the multiple interacting and conforming bad data, strongly interacting topology and analog measurement errors may not be identified due to error masking. Such cases are however rare and cannot be handled by this method.

Table 4.5 Multiple Error Identification Results - 14-bus System

Test A		Test B	
<i>Measurement/Topology</i>	<i>Normalized residual / <math>\lambda^N</math></i>	<i>Measurement/Topology</i>	<i>Normalized residual / <math>\lambda^N</math></i>
$CB_{31-26}$	278.72	$P_{28-26}$	277.83
$P_{31-50}$	174.00	$CB_{31-26}$	219.81
$P_{31-26}$	174.00	$P_{31-50}$	180.60
$CB_{44-42}$	144.64	$P_{31-26}$	180.60
$CB_{45-42}$	212.03	$CB_{44-42}$	133.26

### 4.3 Computation Time

The number of state variables of this implicit topology error identification method is less than the state variables used in traditional state estimation, since it is based only on the real power flow measurements. The computation times for the topology error analysis program and the traditional state estimation program are given in Table 4.6 for the test systems. Note that the topology error analysis method uses the detailed substation topology data for all the buses.

Table 4.6 Comparison of Computation time

Test System	Computation Time (Sec.)	
	Topology Error Analysis	State Estimation
14-bus	0.8750	0.5780
30-bus	1.1560	0.8120
57-bus	4.1250	2.682

For all three systems, the computation time of topology error analysis program is almost 150% of the traditional state estimation. Considering the complexity of the substation level system, this result is acceptable.

## 5. Program Data Structure

---

The input data files for the topology analysis program include the detailed circuit breaker connection information and the power flow measurements through the circuit breakers. The output data files give the normalized Lagrange multipliers of CBs constraints and the normalized residuals of measurements.

### 5.1 Input Data Files

The input data of the topology analysis is composed of three files: (1) the detailed circuit breaker topology data, (2) power flow measurement data, and (3) voltage data.

#### 5.1.1 topoanainput.dat

```
1 4 6 1 15 16 17
2 6 10 2 18 19 20 21 22
3 4 6 3 23 24 25
4 7 13 4 26 27 28 29 30 31
5 6 10 5 32 33 34 35 36
6 6 10 6 37 38 39 40 41
7 5 8 7 42 43 44 45
8 1 1 8
9 6 10 9 46 47 48 49 50
10 4 6 10 51 52 53
11 4 6 11 54 55 56
12 4 6 12 57 58 59
13 5 8 13 60 61 62 63
14 4 6 14 64 65 66
-99
1 0 -1 0 1.000 1 2 16 19 0.01938 0.05917 0.00000 0.05280
2 0 -1 0 1.000 1 5 17 33 0.05403 0.22304 0.00000 0.04920
3 0 -1 0 1.000 2 5 20 34 0.05695 0.17388 0.00000 0.03400
4 0 -1 0 1.000 2 4 21 27 0.05811 0.17632 0.00000 0.03740
5 0 -1 0 1.000 2 3 22 24 0.04699 0.19797 0.00000 0.04380
6 0 -1 0 1.000 3 4 25 28 0.06701 0.17103 0.00000 0.03460
7 0 -1 0 1.000 4 5 29 35 0.01335 0.04211 0.00000 0.01280
8 0 -1 0 1.000 7 8 43 8 0.00000 0.17615 0.00000 0.00000
9 0 -1 0 1.000 7 9 44 47 0.00000 0.11001 0.00000 0.00000
10 0 -1 0 1.000 9 10 48 52 0.03181 0.08450 0.00000 0.00000
11 0 -1 0 1.000 9 14 49 65 0.12711 0.27038 0.00000 0.00000
12 0 -1 0 1.000 6 11 38 55 0.09498 0.19890 0.00000 0.00000
13 0 -1 0 1.000 6 12 39 58 0.12291 0.25581 0.00000 0.00000
14 0 -1 0 1.000 6 13 40 61 0.06615 0.13027 0.00000 0.00000
15 0 -1 0 1.000 12 13 59 62 0.22092 0.19988 0.00000 0.00000
16 0 -1 0 1.000 13 14 63 66 0.17093 0.34802 0.00000 0.00000
17 0 -1 1 0.930 6 5 41 36 0.00000 0.25202 0.00000 0.00000
18 0 -1 1 0.960 9 4 50 30 0.00000 0.55618 0.00000 0.00000
19 0 -1 1 0.970 4 7 31 45 0.00000 0.20912 0.00000 0.00000
20 0 -1 0 1.000 10 11 53 56 0.08205 0.19207 0.00000 0.00000
21 1 1 -1 -1 -1 -1 1 16 0.00000 0.00000 0.00000 0.00000
22 1 1 -1 -1 -1 -1 16 15 0.00000 0.00000 0.00000 0.00000
23 1 0 -1 -1 -1 -1 1 17 0.00000 0.00000 0.00000 0.00000
24 1 1 -1 -1 -1 -1 17 15 0.00000 0.00000 0.00000 0.00000
25 2 1 -1 -1 -1 -1 2 19 0.00000 0.00000 0.00000 0.00000
26 2 0 -1 -1 -1 -1 19 20 0.00000 0.00000 0.00000 0.00000
27 2 1 -1 -1 -1 -1 20 18 0.00000 0.00000 0.00000 0.00000
28 2 1 -1 -1 -1 -1 2 21 0.00000 0.00000 0.00000 0.00000
29 2 1 -1 -1 -1 -1 21 22 0.00000 0.00000 0.00000 0.00000
30 2 1 -1 -1 -1 -1 22 18 0.00000 0.00000 0.00000 0.00000
.....
-99
```

The file shown above is part of the topoanainput.dat file of 14 bus system. This input file includes the detailed circuit breaker topology information. -99 is used to flag of the end of data. It is composed of two parts, the substation information data and the circuit breaker topology of the system.

### Substation Information Data

1st column: substation number.

2nd column: total number of electrical nodes included in that substation.

3rd column: total number of branches belong to that substation. It includes all the circuit breakers and the non-zero impedance branches connected to this station.

4th column to the end: the number of columns after the 3rd column differs for each substation, it shows the detailed electrical node number of that substation.

### Circuit Breaker Topology Data

1st column: the branch number.

2nd column: the substation number of that line. For non-zero impedance branch, the value is 0. For circuit breakers, the value is the number of the substation it belongs to.

3rd column: circuit breaker status. For non-zero impedance branch, the value is -1. For open circuit breakers, the value is 0. For closed circuit breakers, the value is 1.

4th column: the line type. For a transformer, the value is 1 and for a normal transmission line, the value is 0. For circuit breakers, the value is -1.

5th column: tap value. For a transformer, it gives the tap value of that transformer. For normal transmission line it is 1. For circuit breaker it is -1.

6th to 7th columns: the start and end substation number the non-zero impedance branch connected. For circuit breakers, the value is -1.

8th to 9th columns: the detailed electrical nodes of a branch, for both the non-zero impedance branch and circuit breaker.

10th to 13th columns: the resistance, reactance, conductance and susceptance of the non-zero impedance branch. For circuit breakers, the values will be all zeros.

#### 5.1.2 topomeasure.dat

1	1	1	16	19	1.572330	0.000001
1	1	2	17	33	0.754130	0.000001
1	1	21	1	16	2.326470	0.000001
1	1	22	16	15	0.754140	0.000001
1	1	24	17	15	-0.754130	0.000001
1	2	5	22	24	0.736110	0.000001
1	2	1	19	16	-1.529160	0.000001

1	2	3	20	34	0.411410	0.000001
1	2	4	21	27	0.564670	0.000001
1	2	25	2	19	-1.529160	0.000001
1	2	27	20	18	-0.411410	0.000001
1	2	28	2	21	1.712160	0.000001
1	2	29	21	22	1.147520	0.000001
1	2	30	22	18	0.411410	0.000001
1	3	6	25	28	-0.229230	0.000001
1	3	5	24	22	-0.712640	0.000001
1	3	31	3	24	-0.942000	0.000001
1	3	32	24	23	-0.229360	0.000001
1	3	34	25	23	0.229230	0.000001

.....

-99						
3	1	1	2.326470		0.000001	
3	2	2	0.183000		0.000001	
3	3	3	-0.942000		0.000001	
3	4	4	-0.478000		0.000001	
3	5	5	-0.076000		0.000001	
3	6	6	-0.112000		0.000001	
3	7	7	0.000000		0.000001	
3	8	8	0.000000		0.000001	
3	9	9	-0.295000		0.000001	
3	10	10	-0.090000		0.000001	
3	11	11	-0.035000		0.000001	
3	12	12	-0.061000		0.000001	
3	13	13	-0.135000		0.000001	
3	14	14	-0.149000		0.000001	
-99						

The list shown above is part of the topomeasure.dat file for the 14 bus system. Since the topology analysis method only uses the real power flow and injection data, both directions of power flows of a non-zero impedance branch and all of the bus real power injections are needed in order to give enough redundancy. It is composed of two parts.

### Power Flow Measurements

1st column: the flag of the measurement. 1 represents it is a real power flow measurement.

2nd column: the station number that power flow belongs to, whether it is a non-zero impedance branch connected to that station or it is a circuit breaker in that station.

3rd column: the branch number of that power flow.

4th to 5th columns: the start and end node number of that power flow.

6th column: the power flow measurement.

7th column: the weight of that measurement.

### Power Injection Measurements

1st column: the flag of the measurement. 3 represents it is a real power injection measurement.

2nd column: the substation number of that power injection belongs to.

3rd column: the node number of that power injection.

4th column: the power injection measurement.

5th column: the weight of that measurement.

### 5.1.3 vinput.dat

1	1.0600
2	1.0450
3	1.0100
4	1.0137
5	1.0211
6	1.0269
7	1.0109
8	1.0512
9	0.9860
10	0.9753
11	0.9687
12	1.0096
13	1.0023
14	0.9739
-99	

This file contains the state estimation results for all the bus voltage magnitudes. They are supplied to be used in the topology analysis program since the node voltages will not be included in the state variables.

1st column: the substation number.

2nd column: the magnitude of the voltage.

### 5.2 Output Data Files

There is only one output file of the topology analysis program. A sample is shown below.

BADDATAOTP.dat

The maximum normalized lagrange multiplier

55	54	221.6456
----	----	----------

Normalized lagrange multiplier

1	16	19.2210
---	----	---------

16	15	11.4732
17	15	11.4732
1	17	0.5939
2	19	19.8892
20	18	11.0035
2	21	19.8892
22	18	11.0035
21	22	15.7338
19	20	13.7105
3	24	0.0000
24	23	11.9863
25	23	11.9863
3	25	6.6629
4	27	91.8836
28	26	99.9550
27	28	94.9610
4	29	91.8836
30	26	72.7250
31	26	93.7364
29	30	72.2868
4	31	72.0833
5	33	10.3829
34	32	16.4818
5	35	10.3829
36	32	16.4818
35	36	78.7925

.....

Normalized residual

1	16	19	3.6377
1	17	33	8.5261
1	1	16	12.2294
1	16	15	8.5161
1	17	15	19.6174
3	1		12.2294
1	22	24	0.9091
1	19	16	6.5413
1	20	34	8.1585
1	21	27	1.1742
1	2	19	6.5413
1	20	18	1.1277
1	2	21	8.3697
1	21	22	9.2521
1	22	18	8.1585
3	2		2.4140
1	25	28	1.4052
1	24	22	1.0737
1	3	24	2.7164
1	24	23	1.2694
1	25	23	5.4512
3	3		2.7164
1	27	21	0.0584
1	31	45	23.7211
1	30	50	14.0347

1 29 35 38.5945  
.....

This file gives the normalized Lagrange multipliers of the CB constraints and normalized residuals of the measurements.

### **The Maximum Normalized Lagrange Multiplier**

1st to 2nd columns: the start and end node number of the circuit breaker.

3rd column: the normalized Lagrange multiplier of that CB constraint, which is the largest one of all.

### **Normalized Lagrange Multiplier**

1st to 2nd columns: the start and end node number of the circuit breaker.

3rd column: the normalized Lagrange multiplier of that CB constraint.

### **Normalized Residual**

1st column: the flag of the measurement. 1 represents it is a real power flow measurement. 3 represents it is a real power injection measurement.

For real power flow measurement

2nd to 3rd columns: the start and end node number of that power flow measurement.

4th column: normalized residual of that measurement.

### **For Real Power Injection Measurement**

2nd column: the connected node number of that power injection measurement.

3rd column: normalized residual of that measurement.

## 6. Conclusions and Future Work

---

This project demonstrates that the presented topology error analysis method provides a viable and efficient solution for large power systems. This method can identify network topology error even in the presence of bad measurements. The topology error identification is accomplished by formulating the circuit breaker variables as zero equality constraints and then testing the significance of the associated Lagrange multipliers. These are computed from the normalized measurement residuals obtained by the process similar to the traditional state estimation. The method provides enough flexibility treating different scales of substation level topology. Only one substation or all substations can be modeled in detail at the substation level without significant computational burden. By using the implicit model, most of the variables are treated as equality constraints and thus are excluded from the estimation equations. The state variables will thus be not significantly more than the number of state variables in the traditional state estimation. The computation time increases roughly 50% compared to the traditional state estimation solution, which is quite acceptable considering the fact that the entire substation is represented in detail.

A natural extension of this work is to consider the same approach for parameter error detection and identification. Preliminary studies conducted as part of this project indicate promising results. The advantage of such an extension is that any sort of parameter errors or biases, such as those associated with sagging transmission lines, or missing transformer taps, etc. can be detected without requiring any prior knowledge or suspicion about these parameters. Furthermore, the procedure will facilitate simultaneous detection of bad data and parameter errors, enabling differentiation between occasional bad data and systematic errors due to wrong parameters.

## REFERENCES

---

- [1] Aboytes F., Cory B., "Identification of Measurement, Parameter and Configuration Errors in Static State Estimation." *PICA Conference Proceedings*, pp. 298-302, June 1975.
- [2] Abur A., H. Kim, Çelik M., "Identifying the Unknown Circuit Breaker Statuses in Power Networks," *IEEE Transactions on Power Systems*, Vol. 10(4), pp. 2029-2037, November 1995.
- [3] Alsac O., Vempati N., Stott B., Monticelli A., "Generalized State Estimation," *IEEE Transactions on Power Systems*, Vol. 13, No. 3, pp. 1069-1075, August 1998.

- [4] Clements K.A., Simoes-Costa A., "Topology Error Identification Using Normalized Lagrange Multipliers," *IEEE Transactions on Power Systems*, Vol. 13(2), pp. 347-353, May 1998.
- [5] Clements K.A., Davis P. W., "Detection and Identification of Topology Errors in Electric Power Systems," *IEEE Transactions on Power Systems*, Vol. 3, No. 4, pp. 1748-1753, November 1988.
- [6] Villa de la Jaen, A. and Gómez-Expósito, A., "Implicitly constrained substation model for state estimation," *IEEE Transactions on Power Systems*, vol. 17, no. 3, pp. 850-856, Aug. 2002.

## APPENDIX 1. Matlab Code of the Method

---

```
% start to input data
clear all
threshold=1e-3;

finput=fopen('vinput.dat');

ReadLine=fgets(finput);
BranchData=str2num(ReadLine);
I=1;
while BranchData(1)~=-99
    busv(I) = BranchData(1);
    voltage(I) = BranchData(2);
    ReadLine=fgets(finput);
    BranchData=str2num(ReadLine);
    I=I+1;
end

finput=fopen('topoanainput.dat'); % input system network data

ReadLine=fgets(finput);
BranchData=str2num(ReadLine);
I=1;
while BranchData(1)~=-99
    busnum(I) = BranchData(2)+1;
    linenum(I) = BranchData(3);
    bn=busnum(I)-1;
    for x=1:bn
        buscont(I,x)=BranchData(3+x);
    end
    ReadLine=fgets(finput);
    BranchData=str2num(ReadLine);
    I=I+1;
end
total_bus=I-1;

ReadLine=fgets(finput);
BranchData=str2num(ReadLine);
I=1;
while BranchData(1)~=-99
    station(I) = BranchData(2);
    stat(I) = BranchData(3);
    linetype(I) = BranchData(4);
    linetap(I) = BranchData(5);
    startbus(I) = BranchData(6);
    endbus(I) = BranchData(7);
    startnode(I) = BranchData(8);
    endnode(I) = BranchData(9);
    liner(I)=BranchData(10);
    linex(I)=BranchData(11);
    con(I)=BranchData(12);
    sup(I)=BranchData(13);
```

```

        ReadLine=fgets(fininput);
        BranchData=str2num(ReadLine);
        I=I+1;
end
total_line=I-1;

fclose(fininput);

fininput=fopen('topomeasure.dat');           % input measurement data

ReadLine=fgets(fininput);
BranchData=str2num(ReadLine);
I=1;
while BranchData(1)~= -99
    stationpflow(I)=BranchData(2);
    linenumflow(I) = BranchData(3);
    startbuspflow(I) = BranchData(4);
    endbuspflow(I) = BranchData(5);
    measurepflow(I) = BranchData(6);
    measureweightpflow(I) = BranchData(7);
    ReadLine=fgets(fininput);
    BranchData=str2num(ReadLine);
    I=I+1;
end
total_pflow=I-1;

ReadLine=fgets(fininput);
BranchData=str2num(ReadLine);
I=1;
while BranchData(1)~= -99
    stationpinj(I)=BranchData(2);
    buspinj(I) = BranchData(3);
    measurepinj(I) = BranchData(4);
    measureweightpinj(I) = BranchData(5);
    ReadLine=fgets(fininput);
    BranchData=str2num(ReadLine);
    I=I+1;
end
total_pinj=I-1;

[a,bussort]=sort(busv);
V=ones(sum(busnum)-total_bus,1);
for p=1:total_bus
    for x=1:busnum(p)-1
        V(buscont(p,x))=voltage(bussort(p));
    end
end

linez=zeros(total_line,1);           % build line parameter matrix
zthet=zeros(total_line,1);
for x=1:total_line
    if linetype(x)==1
        linez(x)=linex(x)*linetap(x);
        zthet(x)=pi/2;
    else

```

```

        linez(x)=sqrt(liner(x)^2+linex(x)^2);
        if liner(x)~=0
            zthet(x)=atan(linex(x)/liner(x));
        else
            if linex(x)>0
                zthet(x)=pi/2;
            else
                zthet(x)=-pi/2;
            end
        end
    end
end

fclose(finput);

for p=1:total_bus
    temp=find(stationpflow==p);
    [a,b]=size(temp);
    flownum(p)=b;
    temp=find(stationpinj==p);
    [a,b]=size(temp);
    injnum(p)=b;
    linknum(p)=linenum(p)+injnum(p)-busnum(p)+1;
end
Plcom1=zeros(max(flownum)+max(injnum),max(linknum),total_bus);
Plcom2=zeros(max(flownum)+max(injnum),max(linknum),total_bus);
thetacom=zeros(max(linknum),max(busnum)-1,total_bus);

close=zeros(total_bus,1);
open=zeros(total_bus,1);
thresh=zeros(total_bus,1);
varnum=zeros(total_bus,1);
flag=0;
tree=zeros(1,2);
bp=find(stat==-1);
[a,bpsize]=size(bp);

for p=1:total_bus
    substation
        if busnum(p)>2
            A=zeros(busnum(p),linenum(p)+total_pinj);
            m=1;
            for x=1:total_pinj
                if stationpinj(x)==p
                    A(1,m)=1;
                    for y=1:busnum(p)-1
                        if buscont(p,y)==buspinj(x)
                            A(y+1,m)=-1;
                            tree(p,m)=total_line+x;
                            m=m+1;
                        end
                    end
                end
            end
        end
    end
end
end

```

```

for x=1:total_line
    if station(x)==p & stat(x)==1
        for y=1:busnum(p)-1
            if buscont(p,y)==startnode(x)
                A(y+1,m)=1;
            end
            if buscont(p,y)==endnode(x)
                A(y+1,m)=-1;
            end
            tree(p,m)=x;
        end
        close(p)=close(p)+1;
        m=m+1;
    end
end
thresh(p)=m-1;
for x=1:total_line
    if station(x)==p & stat(x)==0
        for y=1:busnum(p)-1
            if buscont(p,y)==startnode(x)
                A(y+1,m)=1;
            end
            if buscont(p,y)==endnode(x)
                A(y+1,m)=-1;
            end
            tree(p,m)=x;
        end
        open(p)=open(p)+1;
        m=m+1;
    end
end
varnum(p)=m-1;

ground=0;
for x=1:busnum(p)-1
    if A(x,x)==0
        for y=x+1:m
            if A(x,y)~=0
                A(:,x:y)=[A(:,y) A(:,x:y-1)];
                tree(p,x:y)=[tree(p,y) tree(p,x:y-1)];
                if ground==0
                    if y>x & y<=x+injnum(p)-1

A(:,x+1:thresh(p))=[A(:,x+injnum(p):thresh(p)) A(:,x+1:x+injnum(p)-1)];

tree(p,x+1:thresh(p))=[tree(p,x+injnum(p):thresh(p))
tree(p,x+1:x+injnum(p)-1)];

                    ground=1;
                end
            end
            break
        end
    end
else
    if ground==0

```

```

        A(:,x+1:thresh(p))=[A(:,x+injnum(p):thresh(p))
A(:,x+1:x+injnum(p)-1)];
        tree(p,x+1:thresh(p))=[tree(p,x+injnum(p):thresh(p))
tree(p,x+1:x+injnum(p)-1)];
        ground=1;
    end
end
A(x,x+1:m)=A(x,x+1:m)./A(x,x);
for y=x+1:busnum(p)
    for z=x+1:m
        A(y,z)=A(y,z)-A(x,z)*A(y,x);
    end
end
end

AA=zeros(busnum(p),linenum(p)+injnum(p));
for x=1:m-1
    y=tree(p,x);
    if y>total_line
        y=y-total_line;
        AA(1,x)=1;
        for z=1:busnum(p)-1
            if buscont(p,z)==buspinj(y)
                AA(z+1,x)=-1;
            end
        end
    else
        for z=1:busnum(p)-1
            if buscont(p,z)==startnode(y)
                AA(z+1,x)=1;
            end
            if buscont(p,z)==endnode(y)
                AA(z+1,x)=-1;
            end
        end
    end
end
end
x=m;
for y=1:total_line
    if (stat(y)==-1) & (startbus(y)==p | endbus(y)==p)
        node=0;
        for z=1:busnum(p)-1
            if buscont(p,z)==startnode(y)
                AA(z+1,x)=1;
                node=1;
            end
            if buscont(p,z)==endnode(y)
                AA(z+1,x)=-1;
                node=-1;
            end
        end
    end
    if node==1
        AA(1,x)=-1;
    else
        AA(1,x)=1;
    end
end

```

```

        end
        tree(p,x)=y;
        x=x+1;
    end
end
AA=AA(1:busnum(p)-1,:);
At=AA(:,1:busnum(p)-1);
Al=AA(:,busnum(p):linenum(p)+injnum(p));
Dl=inv(At)*Al;
Bt=-Dl';
B=[Bt eye(linknum(p))];

nonzerobranch(p)=linenum(p)+injnum(p)-m+1;
z=1;
for y=1:bpsize
    if startbus(y)==p | endbus(y)==p
        nonbp(p,z)=y;
        z=z+1;
    end
end
Pcom=B';
[a,b]=size(Pcom);
Pflowcom=zeros(flownum(p)+injnum(p),b);
y=1;
for x=1:total_pflow
    if stationpflow(x)==p
        if startbuspflow(x)==startnode(linenum_pflow(x))
Pflowcom(y,:)=Pcom(find(tree(p,:)==linenum_pflow(x)),:);
            else
                Pflowcom(y,:)=
Pcom(find(tree(p,:)==linenum_pflow(x)),:);
            end
            y=y+1;
        end
    end
    for x=1:total_pinj
        z=x+total_line;
        if stationpinj(x)==p
            Pflowcom(y,:)=Pcom(find(tree(p,:)==z),:);
            y=y+1;
        end
    end
    Plcom1(1:flownum(p)+injnum(p),1:linknum(p)-
nonzerobranch(p),p)=Pflowcom(:,1:linknum(p)-nonzerobranch(p));

    Plcom2(1:flownum(p)+injnum(p),1:nonzerobranch(p),p)=Pflowcom(:,linknum(p)-
nonzerobranch(p)+1:linknum(p));
    thetacom(1:nonzerobranch(p),1:busnum(p)-1,p)=-Bt(linknum(p)-
nonzerobranch(p)+1:linknum(p),:);
    else
        [a,b]=size(tree); % for substation with only 1 out
lines
        tree(p,:)=zeros(1,b);
        for x=1:total_pflow

```

```

        if startbuspflow(x)==p | endbuspflow(x)==p
            flag=1;
        end
    end
end
if flag==1
    y=0;
    for x=1:total_line
        if station(x)==0
            if startbus(x)==p
                thetacom(y+1,1,p)=-1;
                y=y+1;
            end
            if endbus(x)==p
                thetacom(y+1,1,p)=1;
                y=y+1;
            end
        end
    end
    end
    nonzerobranch(p)=y;
    z=1;
    for y=1:bpsize
        if startbus(y)==p | endbus(y)==p
            nonbp(p,z)=y;
            z=z+1;
        end
    end
    end
    y=0;
    for x=1:total_pflow
        if stationpflow(x)==p
            if startbuspflow(x)==startnode(linenumflow(x))
                a=linenumflow(x);
                for z=1:nonzerobranch(p)
                    if nonbp(p,z)==a
                        Plcom2(1+y,z,p)=1;
                    end
                end
                y=y+1;
            else
                a=linenumflow(x);
                for z=1:nonzerobranch(p)
                    if nonbp(p,z)==a
                        Plcom2(1+y,z,p)=-1;
                    end
                end
                y=y+1;
            end
        end
    end
    end
    for x=1:total_pinj
        if stationpinj(x)==p
            temp=cumsum(Plcom2(1:y,: ,p));
            Plcom2(1+y,: ,p)=temp(y,:);
        end
    end
    end
    varnum(p)=1;

```

```

        flag=0;
    end
end
end

for p=1:total_bus
    for x=1:nonzerobranch(p)
        for y=1:busnum(p)-1
            if thetacom(x,y,p)~=0
                if tree(p,y)<total_line & tree(p,y)~=0
                    if stat(tree(p,y))==0
                        thetacom(x,:,p)=zeros(1,max(busnum)-1);
                    end
                end
            end
        end
    end
end

end

variable=zeros(sum(varnum),1);

delta=1;
threshold=1e-3;

H=zeros(total_pflow+total_pinj,sum(varnum));

while delta>=threshold           % state estimation part
    startrow=0;
    startcol=0;
    x=0;
    y=0;
    deltaz=zeros(sum(flownum)+sum(injnum),1);
    for p=1:total_bus
        deltaz(1+x+y:x+y+flownum(p))=measurepflow(1+x:x+flownum(p));
        x=x+flownum(p);
        deltaz(1+x+y:x+y+injnum(p))=measurepinj(1+y:y+injnum(p));
        y=y+injnum(p);
    end
    for p=1:total_bus           % build Jacobian matrix
        for x=1:flownum(p)+injnum(p)
            for y=1:nonzerobranch(p)
                temp1=Plcom2(x,y,p)*thetacom(y,1:busnum(p)-1,p);
                n=nonbp(p,y);
                if startbus(n)==p
                    q=endbus(n);
                else
                    q=startbus(n);
                end
                for v=1:nonzerobranch(q)
                    if nonbp(q,v)==n
                        node=v;
                    end
                end
            end
            if Plcom2(x,y,p)==1
                temp2=thetacom(node,1:busnum(q)-1,q);
            end
        end
    end
    delta=norm(H\variable);
end

```

```

        from=startnode(n);
        to=endnode(n);
    elseif Plcom2(x,y,p)==-1
        temp2=(-1)*thetacom(node,1:busnum(q)-1,q);
        from=endnode(n);
        to=startnode(n);
    else
        temp2=0*thetacom(node,1:busnum(q)-1,q);
    end
    startq=0;
    for v=1:q-1
        startq=startq+varnum(v);
    end
    if nnz(temp1)~=0 & nnz(temp2)~=0
        for z=1:busnum(p)-1

H(startrow+x,startcol+z)=H(startrow+x,startcol+z)+temp1(z)*V(from)*V(to)*s
in(temp1*variable(startcol+1:startcol+busnum(p)-
1)+temp2*variable(startq+1:startq+busnum(q)-1)+zthet(n))/linez(n);
            end
            for z=1:busnum(q)-1

H(startrow+x,startq+z)=temp2(z)*V(from)*V(to)*sin(temp1*variable(startcol+
1:startcol+busnum(p)-1)+temp2*variable(startq+1:startq+busnum(q)-
1)+zthet(n))/linez(n);
                end
                deltaz(startrow+x)=deltaz(startrow+x)-
V(from)*(V(from)*cos(zthet(n))-
V(to)*cos(temp1*variable(startcol+1:startcol+busnum(p)-
1)+temp2*variable(startq+1:startq+busnum(q)-1)+zthet(n)))/linez(n);
                    end
                    if busnum(p)>2
                        deltaz(startrow+x)=deltaz(startrow+x)-
Plcom1(x,1:linknum(p)-
nonzerobranch(p),p)*variable(startcol+busnum(p):startcol+varnum(p));
                            end
                            end
                            if busnum(p)>2

H(startrow+1:startrow+flownum(p)+injnum(p),startcol+busnum(p):startcol+var
num(p))=Plcom1(1:flownum(p)+injnum(p),1:linknum(p)-nonzerobranch(p),p);
                                end
                                startrow=startrow+flownum(p)+injnum(p);
                                startcol=startcol+varnum(p);
                            end

startcol=0;
y=1;
z=1;
cbnum=0;
pxinum=0;
cbnumber=zeros(total_bus,1);
for p=1:total_bus
two parts
                    % divide the Jacobian matrix into

```

```

        if busnum(p)>2                                % Hi and Hcb according to the tree
determined
        for x=1:busnum(p)-1
            if tree(p,x)<=total_line & stat(tree(p,x))==1
                Hcb(:,y)=H(:,startcol+x);
                cb(p,y-cbnum)=tree(p,x);
                y=y+1;
            else
                if tree(p,x)>total_line | stat(tree(p,x))~=0
                    Hi(:,z)=H(:,startcol+x);
                    pxi(z)=startcol+x;
                    z=z+1;
                end
            end
        end
        for x=busnum(p):varnum(p)
            if tree(p,x)<=total_line & stat(tree(p,x))==0
                Hcb(:,y)=H(:,startcol+x);
                cb(p,y-cbnum)=tree(p,x);
                y=y+1;
            elseif tree(p,x)<=total_line & stat(tree(p,x))==1
                Hi(:,z)=H(:,startcol+x);
                pxi(z)=startcol+x;
                z=z+1;
                cb(p,y-cbnum)=tree(p,x);
                y=y+1;
            else
                if tree(p,x)>total_line
                    Hi(:,z)=H(:,startcol+x);
                    pxi(z)=startcol+x;
                    z=z+1;
                end
            end
        end
    else
        for x=1:total_pflow
            if startbuspflow(x)==p | endbuspflow(x)==p
                flag=1;
            end
        end
        if flag==1
            Hi(:,z)=H(:,startcol+1);
            pxi(z)=startcol+1;
            z=z+1;
            flag=0;
        end
    end
    startcol=startcol+varnum(p);
    cbnum=y-1;
    cbnumber(p)=cbnum-sum(cbnumber);
end

[m,n]=size(Hi);
Hi=Hi(:,2:n);

```

```

Ro=[measureweightpflow';measureweightpinj'];
Hp=Hi;
Hg=Hcb;

Ci=Hp;
ci=deltaz;
Ccb=Hg;
cnumber=zeros(sum(injnum),1);

y=0;
z=0;
q=0;
cn=1;
for p=1:total_bus % excluded the zero injection constraints
from H matrix
    x=flownum(p);
    Ci(q+1:x+q,:)=[];
    ci(q+1:x+q,:)=[];
    Ccb(q+1:x+q,:)=[];
    y=y+flownum(p);
    x=injnum(p);
    qq=0;
    while x>0
        if measurepinj(z+x)~=0
            Ci(x+q,:)=[];
            ci(x+q,:)=[];
            Ccb(x+q,:)=[];
        else
            Hp(x+y,:)=[];
            Hg(x+y,:)=[];
            Ro(x+y)=[];
            deltaz(x+y)=[];
            cnumber(cn)=z+x;
            cn=cn+1;
            qq=qq+1;
        end
        x=x-1;
    end
    q=q+qq;
    y=y+injnum(p)-qq;
    z=z+injnum(p);
end

R=diag(Ro); % computation of r and mu
W=inv(R);
[m,n]=size(Hp);
[p,q]=size(Ci);
G=[zeros(n,n) Hp'*W Ci';Hp eye(m) zeros(m,p);Ci zeros(p,m)
zeros(p,p)];
vec=[zeros(n,1);deltaz;ci];
Lag=inv(G);
quest=Lag*vec;

deltaxi=quest(1:n);
delta=max(abs(deltaxi));

```

```

    for x=1:n
        variable(pxi(x+1))=variable(pxi(x+1))+deltaxi(x);
    end
end

mu=quest(n+1:n+m+p);
T=-[Hg'*W' Ccb']; % compute lumda
lumda=T*mu;
E1=Lag(n+1:n+m,n+1:n+m);
E2=Lag(1+n+m:n+m+p,n+1:n+m);
cov=[E1;E2];
covr=cov*R*cov';
covlumda=T*covr*T';
[a,b]=size(Hcb);
lumdan=zeros(b,1); % normalize lumda
for x=1:b
    if covlumda(x,x)~=0
        lumdan(x)=abs(lumda(x)/sqrt(covlumda(x,x)));
    end
end

r=quest(n+1:n+m+p); % normalize r
rn=zeros(m+p,1);
for x=1:m+p
    if covr(x,x)~=0
        rn(x)=abs(r(x)/sqrt(covr(x,x)));
    end
end

x=cn-1;
zpinj=zeros(cn-1,1);
while x~=0
    zpinj(x)=buspinj(cnumber(x));
    buspinj(cnumber(x))=[];
    x=x-1;
end

for x=1:cn-1
    p=stationpinj(cnumber(x));
    injnum(p)=injnum(p)-1;
end

% Output the results

foutput = fopen('BADATAOTP.dat','w');

fprintf(foutput,'\n\nThe maximum normalized lagrange multiplier \n');
[lumdamax,I]=max(lumdan);
y=0;
for p=1:total_bus
    for x=1:cbnumber(p)
        if I==y+x

```

```

fprintf(foutput, '\n%5d%5d%15.4f', startnode(cb(p,x)), endnode(cb(p,x)), lumda
max);
    end
    end
    y=y+cbnumber(p);
end

fprintf(foutput, '\n\nNormalized lagrange multiplier \n');
y=0;
for p=1:total_bus
    for x=1:cbnumber(p)

fprintf(foutput, '\n%5d%5d%15.4f', startnode(cb(p,x)), endnode(cb(p,x)), lumda
n(y+x));
        end
        y=y+cbnumber(p);
    end

fprintf(foutput, '\n\nNormalized residual \n');
y=0;
z=0;
for p=1:total_bus
    for x=1:flownum(p)

fprintf(foutput, '\n%3d%5d%5d%15.4f', 1, startbuspflow(y+x), endbuspflow(y+x),
rn(y+z+x));
        end
        y=y+flownum(p);
        for x=1:injnum(p)
            fprintf(foutput, '\n%3d%5d%20.4f', 3, buspinj(z+x), rn(y+z+x));
        end
        z=z+injnum(p);
    end

for x=1:cn-1
    fprintf(foutput, '\n%3d%5d%20.4f', 3, zpinj(x), rn(m+x));
end

fprintf(foutput, '\n\n');
fclose(foutput);

```

## APPENDIX 2. Input Data Files Generating Program

---

The input data files for the topology analysis program include the detailed circuit breaker connection information and the power flow measurements through the circuit breakers. For large systems, it is a hard work to get these data by hand according to the complexity of the system. In such cases, this program will be applied to generate the topology analysis input data files from the normal state estimation data to make a test of the large systems.

### A2.1 Standard Substation Model

Since the objective of this program is to generate the data for testing, the specific substation will be given the standard model on the topological structure.

#### A2.1.1 One-line Substation

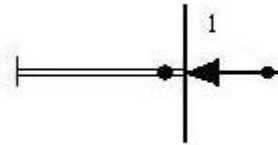


Figure 8.1 One-line Substation Model

There is no circuit breaker in this substation.

### A2.1.2 Two-line Substation

The figure is shown below. There are 4 circuit breakers in this substation.

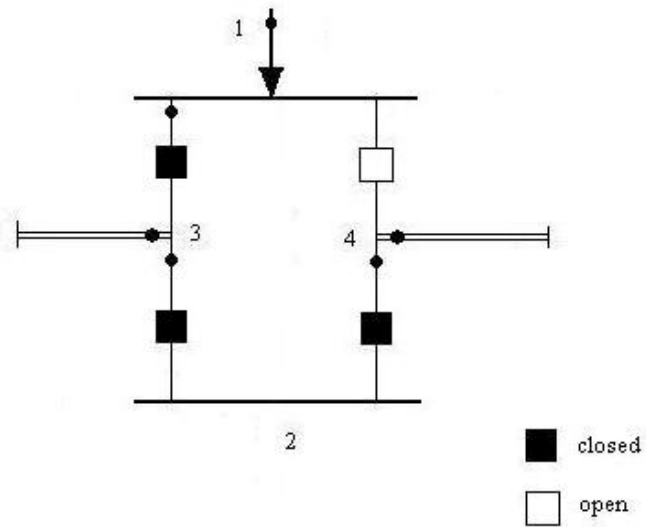


Figure 8.2 Two-line Substation Model

### A2.1.3 Three-line Substation

There are 5 circuit breakers.

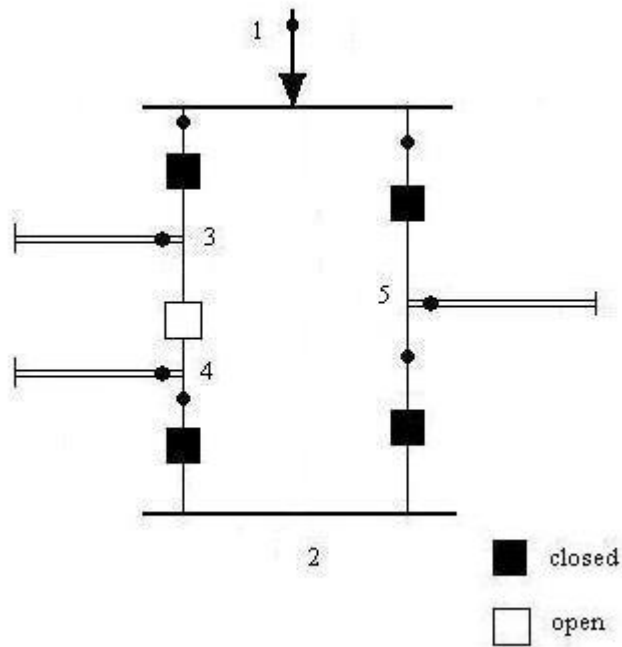


Figure 8.3 Three-line Substation Model

### A2.1.4 Four-line Substation

There are 6 circuit breakers in this substation.

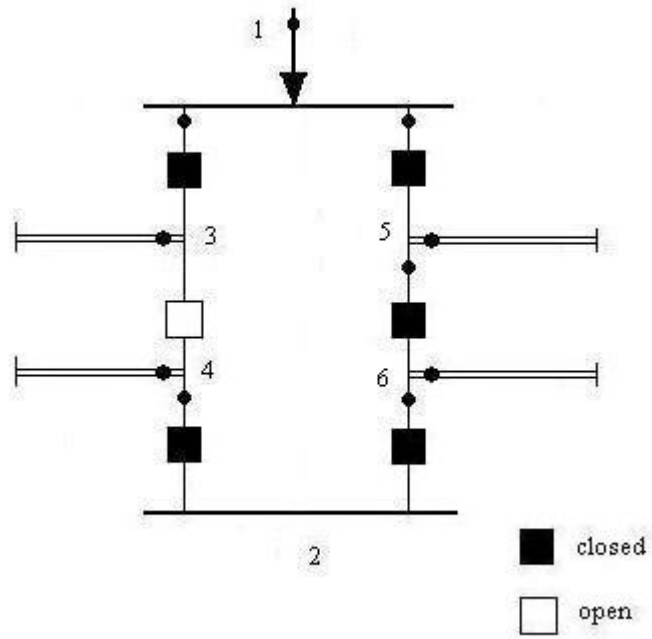


Figure 8.4 Four-line Substation Model

### A2.1.5 Five-line Substation

There are 8 circuit breakers in this substation.

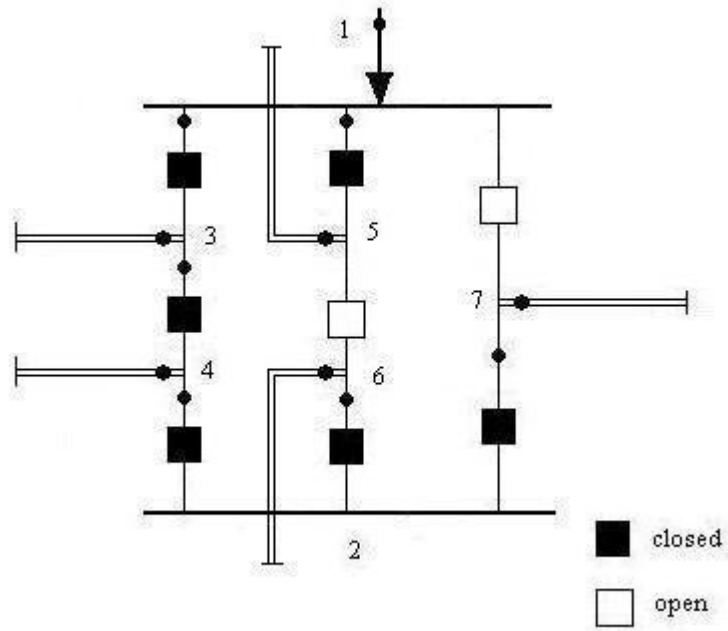


Figure 8.5 Five-line Substation Model

### A2.1.6 Six-line Substation

There are 9 circuit breakers in this substation.

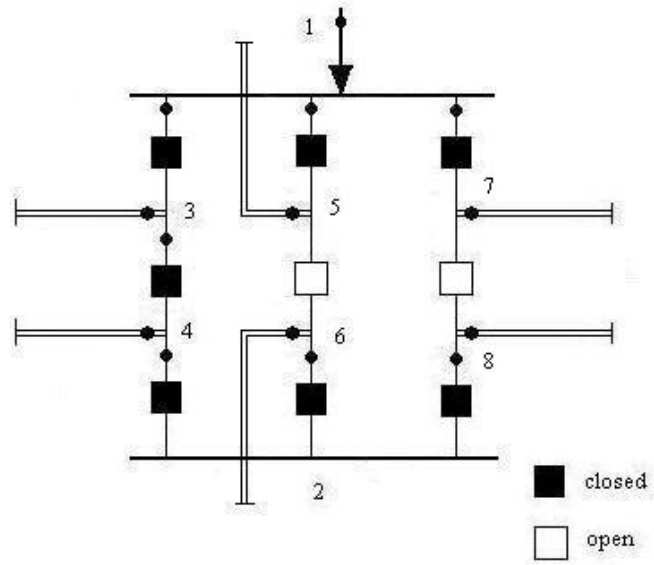


Figure 8.6 Six-line Substation Model

### A2.1.7 Seven-line Substation

There are 11 circuit breakers in this substation.

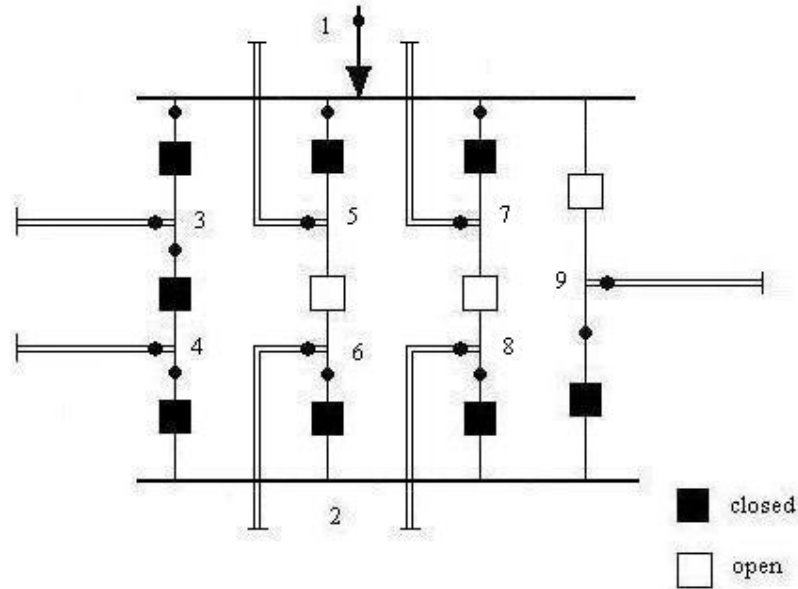


Figure 8.7 Seven-line Substation Model

The power flow measurements of circuit breakers in the specific substation will be calculated according to its own topology.

### A2.2 Input Data Files

The input data is the normal state estimation input data. It is composed of two files, the line parameter data and the measurements data. However, For the purpose of topology analysis, only the real power flow data is needed. And the power flows of both directions of the lines and all of the bus real injections are necessary. The data files of the 14-bus system will be listed below.

#### A2.2.1 seinput.dat

1	1	2	0	1.00000	0.01938	0.05917	0.00000	0.05280
2	1	5	0	1.00000	0.05403	0.22304	0.00000	0.04920
3	2	5	0	1.00000	0.05695	0.17388	0.00000	0.03400
4	2	4	0	1.00000	0.05811	0.17632	0.00000	0.03740
5	2	3	0	1.00000	0.04699	0.19797	0.00000	0.04380
6	3	4	0	1.00000	0.06701	0.17103	0.00000	0.03460
7	4	5	0	1.00000	0.01335	0.04211	0.00000	0.01280
8	7	8	0	1.00000	0.00000	0.17615	0.00000	0.00000
9	7	9	0	1.00000	0.00000	0.11001	0.00000	0.00000
10	9	10	0	1.00000	0.03181	0.08450	0.00000	0.00000
11	9	14	0	1.00000	0.12711	0.27038	0.00000	0.00000

12	6	11	0	1.00000	0.09498	0.19890	0.00000	0.00000
13	6	12	0	1.00000	0.12291	0.25581	0.00000	0.00000
14	6	13	0	1.00000	0.06615	0.13027	0.00000	0.00000
15	12	13	0	1.00000	0.22092	0.19988	0.00000	0.00000
16	13	14	0	1.00000	0.17093	0.34802	0.00000	0.00000
17	10	11	0	1.00000	0.08205	0.19207	0.00000	0.00000
18	6	5	1	0.93000	0.00000	0.25202	0.00000	0.00000
19	4	9	1	0.96000	0.00000	0.55618	0.00000	0.00000
20	4	7	1	0.97000	0.00000	0.20912	0.00000	0.00000

-99

This input file includes the line parameter data. -99 is the flag of the end of the data.

1st column: the line number.

2nd to 3rd columns: the terminal buses of the line.

4th column: the line type. For a transformer, the value is 1 and for a normal transmission line, the value is 0.

5th column: tap value. For a transformer, it gives the tap value of that transformer. For normal transmission lines it is 1.

6th to 9th columns: the resistance, reactance, conductance and susceptance of the branch.

#### A2.2.2 measureinput.dat

1	15	12	13	0.01195	0.000001			
1	12	11	6	-0.05548	0.000001			
1	3	5	2	-0.40324	0.000001			
1	5	2	3	0.73607	0.000001			
1	9	7	9	0.30244	0.000001			
1	14	6	13	0.16723	0.000001			
1	4	4	2	-0.54544	0.000001			
1	1	1	2	1.57062	0.000001			
1	6	3	4	-0.22939	0.000001			
1	8	7	8	0.00000	0.000001			
1	13	6	12	0.07367	0.000001			
1	10	9	10	0.07033	0.000001			
1	11	9	14	0.10972	0.000001			
1	2	1	5	0.75538	0.000001			
1	2	5	1	-0.72781	0.000001			
1	1	2	1	-1.52755	0.000001			
1	8	8	7	0.00000	0.000001			
1	9	9	7	-0.30244	0.000001			
1	17	10	11	-0.02022	0.000001			
1	17	11	10	0.02048	0.000001			
1	16	14	13	-0.04165	0.000001			
1	16	13	14	0.04209	0.000001			
1	15	13	12	-0.01191	0.000001			
1	14	13	6	-0.16520	0.000001			
1	13	12	6	-0.07294	0.000001			
1	12	6	11	0.05590	0.000001			
1	10	10	9	-0.06978	0.000001			

1	3	2	5	0.41211	0.000001
1	4	2	4	0.56233	0.000001
1	5	3	2	-0.71261	0.000001
1	6	4	3	0.23331	0.000001
1	11	14	9	-0.10736	0.000001
1	7	5	4	0.64637	0.000001
1	7	4	5	-0.64098	0.000001
1	19	9	4	-0.17258	0.000001
1	19	4	9	0.17258	0.000001
1	18	6	5	-0.40872	0.000001
1	18	5	6	0.40872	0.000001
1	20	4	7	0.30242	0.000001
1	20	7	4	-0.30242	0.000001
-99					
3	14			-0.14900	0.000001
3	10			-0.09000	0.000001
3	7			0.00000	0.000001
3	8			0.00000	0.000001
3	3			-0.94200	0.000001
3	2			0.18300	0.000001
3	1			2.32600	0.000001
3	11			-0.03500	0.000001
3	12			-0.06100	0.000001
3	13			-0.13500	0.000001
3	6			-0.11200	0.000001
3	9			-0.29500	0.000001
3	4			-0.47800	0.000001
3	5			-0.07600	0.000001
-99					

This input file includes the real power measurements of the line flows and bus injections. It is composed of these two parts.

### Power Flow Data

1st column: the flag of the measurement. 1 represents it is a real power flow measurement.

2nd column: the line number of that power flow.

3rd to 4th columns: The start and end bus number of that power flow.

5th column: the power flow measurement.

6th column: the weight of that measurement.

### Power Injection Data

1st column: the flag of the measurement. 3 represents it is a real power injection measurement.

2nd column: the bus number of that power injection.

3rd column: the power injection measurement.

4th column: the weight of that measurement.

### A2.3 Output Data files

The output data files of this program are the input data of the topology analysis program. It is composed of two files, the detailed CB topology and the CB measurements.

#### A2.3.1 topoanainput.dat

```

1 4 6 1 15 16 17
2 6 10 2 18 19 20 21 22
3 4 6 3 23 24 25
4 7 13 4 26 27 28 29 30 31
5 6 10 5 32 33 34 35 36
6 6 10 6 37 38 39 40 41
7 5 8 7 42 43 44 45
8 1 1 8
9 6 10 9 46 47 48 49 50
10 4 6 10 51 52 53
11 4 6 11 54 55 56
12 4 6 12 57 58 59
13 5 8 13 60 61 62 63
14 4 6 14 64 65 66
-99
1 0 -1 0 1.000 1 2 16 19 0.01938 0.05917 0.00000 0.05280
2 0 -1 0 1.000 1 5 17 33 0.05403 0.22304 0.00000 0.04920
3 0 -1 0 1.000 2 5 20 34 0.05695 0.17388 0.00000 0.03400
4 0 -1 0 1.000 2 4 21 27 0.05811 0.17632 0.00000 0.03740
5 0 -1 0 1.000 2 3 22 24 0.04699 0.19797 0.00000 0.04380
6 0 -1 0 1.000 3 4 25 28 0.06701 0.17103 0.00000 0.03460
7 0 -1 0 1.000 4 5 29 35 0.01335 0.04211 0.00000 0.01280
8 0 -1 0 1.000 7 8 43 8 0.00000 0.17615 0.00000 0.00000
9 0 -1 0 1.000 7 9 44 47 0.00000 0.11001 0.00000 0.00000
10 0 -1 0 1.000 9 10 48 52 0.03181 0.08450 0.00000 0.00000
11 0 -1 0 1.000 9 14 49 65 0.12711 0.27038 0.00000 0.00000
12 0 -1 0 1.000 6 11 38 55 0.09498 0.19890 0.00000 0.00000
13 0 -1 0 1.000 6 12 39 58 0.12291 0.25581 0.00000 0.00000
14 0 -1 0 1.000 6 13 40 61 0.06615 0.13027 0.00000 0.00000
15 0 -1 0 1.000 12 13 59 62 0.22092 0.19988 0.00000 0.00000
16 0 -1 0 1.000 13 14 63 66 0.17093 0.34802 0.00000 0.00000
17 0 -1 0 1.000 10 11 53 56 0.08205 0.19207 0.00000 0.00000
18 0 -1 1 0.930 6 5 41 36 0.00000 0.25202 0.00000 0.00000
19 0 -1 1 0.960 4 9 30 50 0.00000 0.55618 0.00000 0.00000
20 0 -1 1 0.970 4 7 31 45 0.00000 0.20912 0.00000 0.00000
21 1 1 -1 -1 -1 -1 1 16 0.00000 0.00000 0.00000 0.00000
22 1 1 -1 -1 -1 -1 16 15 0.00000 0.00000 0.00000 0.00000
23 1 0 -1 -1 -1 -1 1 17 0.00000 0.00000 0.00000 0.00000
24 1 1 -1 -1 -1 -1 17 15 0.00000 0.00000 0.00000 0.00000
25 2 1 -1 -1 -1 -1 2 19 0.00000 0.00000 0.00000 0.00000
26 2 0 -1 -1 -1 -1 19 20 0.00000 0.00000 0.00000 0.00000
27 2 1 -1 -1 -1 -1 20 18 0.00000 0.00000 0.00000 0.00000
28 2 1 -1 -1 -1 -1 2 21 0.00000 0.00000 0.00000 0.00000
29 2 1 -1 -1 -1 -1 21 22 0.00000 0.00000 0.00000 0.00000
30 2 1 -1 -1 -1 -1 22 18 0.00000 0.00000 0.00000 0.00000
31 3 1 -1 -1 -1 -1 3 24 0.00000 0.00000 0.00000 0.00000
32 3 1 -1 -1 -1 -1 24 23 0.00000 0.00000 0.00000 0.00000
33 3 0 -1 -1 -1 -1 3 25 0.00000 0.00000 0.00000 0.00000
34 3 1 -1 -1 -1 -1 25 23 0.00000 0.00000 0.00000 0.00000
.....
-99

```

This file is the parameter of the circuit breakers in the system. It includes two parts.

### **Substation Information Data**

This data section is about the overall information of the substation.

1st column: substation number.

2nd column: the total number of electrical nodes in the substation.

3rd column: total number of branches belong to that substation. It includes all the circuit breakers and the non-zero impedance branches connected to this station.

4th column to the end: the number of columns after the 3rd column differs for each substation, it shows the detailed node number of that substation.

### **Circuit Breaker Topology Data**

1st column: branch number.

2nd column: station number. For the non-zero impedance branches, it is 0. And for circuit breakers, it is the station number that CB belongs to.

3rd column: CB status. If the CB is open, the value is 0. if it is closed, the value is 1. For the non-zero impedance branches, it is -1.

4th column: the line type. For a transformer, the value is 1 and for a normal transmission line, the value is 0. For circuit breakers, the value is -1.

5th column: tap value. For a transformer, it gives the tap value of that transformer. For normal transmission line it is 1. For circuit breaker it is -1.

6th to 7th columns: the two station numbers connected by a non-zero impedance branch. For the circuit breaker, these values will be set as -1.

8th to 9th columns: the two terminal nodes numbers of a branch, for both the non-zero impedance branch and circuit breaker.

10th to 13th columns: the resistance, reactance, conductance and susceptance of the branch. For the circuit breaker, the values will be all zeros.

#### **A2.3.2 topomeasure.dat**

1	1	1	16	19	1.570620	0.000001
1	1	2	17	33	0.755380	0.000001
1	1	21	1	16	2.326000	0.000001
1	1	22	16	15	0.755380	0.000001
1	1	24	17	15	-0.755380	0.000001
1	2	5	22	24	0.736070	0.000001
1	2	1	19	16	-1.527550	0.000001
1	2	3	20	34	0.412110	0.000001
1	2	4	21	27	0.562330	0.000001
1	2	25	2	19	-1.527550	0.000001

1	2	27	20	18	-0.412110	0.000001
1	2	28	2	21	1.710550	0.000001
1	2	29	21	22	1.148180	0.000001
1	2	30	22	18	0.412110	0.000001
1	3	6	25	28	-0.229390	0.000001
1	3	5	24	22	-0.712610	0.000001
1	3	31	3	24	-0.942000	0.000001
1	3	32	24	23	-0.229390	0.000001
1	3	34	25	23	0.229390	0.000001
.....						
-99						
3	1	1	2.326000		0.000001	
3	2	2	0.183000		0.000001	
3	3	3	-0.942000		0.000001	
3	4	4	-0.478000		0.000001	
3	5	5	-0.076000		0.000001	
3	6	6	-0.112000		0.000001	
3	7	7	0.000000		0.000001	
3	8	8	0.000000		0.000001	
3	9	9	-0.295000		0.000001	
3	10	10	-0.090000		0.000001	
3	11	11	-0.035000		0.000001	
3	12	12	-0.061000		0.000001	
3	13	13	-0.135000		0.000001	
3	14	14	-0.149000		0.000001	
-99						

This file is the detailed power flow measurements through the circuit breaker. It is composed of two parts.

### Power Flow Measurements

1st column: the flag of the measurement. 1 represents it is a real power flow measurement.

2nd column: the station number that power flow belongs to, whether it is a non-zero impedance branch connected to that station or it is a circuit breaker in that station.

3rd column: the branch number of that power flow.

4th to 5th columns: the start and end node number of that power flow.

6th column: the power flow measurement.

7th column: the weight of that measurement.

### Power Injection Measurements

1st column: the flag of the measurement. 3 represents it is a real power injection measurement.

2nd column: the substation number of that power injection belongs to.

3rd column: the node number of that power injection. For the standard model used in this program, this node number will be the same with the substation number.

4th column: the power injection measurement.

5th column: the weight of that measurement.

## A2.4 Matlab Code

```
% start to input data
clear all

finput=fopen('seinput.dat');           % input system network data

ReadLine=fgets(finput);
BranchData=str2num(ReadLine);
I=1;
while BranchData(1)~-=-99
    startbus(I) = BranchData(2);
    endbus(I) = BranchData(3);
    linetype(I)=BranchData(4);
    linetap(I)=BranchData(5);
    liner(I)=BranchData(6);
    linex(I)=BranchData(7);
    con(I)=BranchData(8);
    sup(I)=BranchData(9);
    ReadLine=fgets(finput);
    BranchData=str2num(ReadLine);
    I=I+1;
end
total_line=I-1;
total_bus=max(max(startbus),max(endbus));

fclose(finput);

finput=fopen('measureinput.dat');      % input measurement data

ReadLine=fgets(finput);
BranchData=str2num(ReadLine);
I=1;
while BranchData(1)~-=-99
    linenumflow(I)=BranchData(2);
    startbuspflow(I) = BranchData(3);
    endbuspflow(I) = BranchData(4);
    measurepflow(I) = BranchData(5);
    measureweightpflow(I) = BranchData(6);
    ReadLine=fgets(finput);
    BranchData=str2num(ReadLine);
    I=I+1;
end
total_pflow=I-1;

ReadLine=fgets(finput);
BranchData=str2num(ReadLine);
I=1;
```

```

while BranchData(1)~= -99
    buspinj(I) = BranchData(2);
    measurepinj(I) = BranchData(3);
    measureweightpinj(I) = BranchData(4);
    ReadLine=fgets(fininput);
    BranchData=str2num(ReadLine);
    I=I+1;
end
total_pinj=I-1;

fclose(fininput);

station(1:total_line,1)=zeros(total_line,1);
stat(1:total_line,1)=-ones(total_line,1);
startbuscb(1:total_line,1)=startbus';
endbuscb(1:total_line,1)=endbus';
startnode(1:total_line,1)=zeros(total_line,1);
endnode(1:total_line,1)=zeros(total_line,1);
linenum=total_line;
nodenum=total_bus;

a=0;
b=0;
c=0;
d=0;
for x=1:total_bus % build the substation structure
    [a,b]=size(find(startbus==x));
    [c,d]=size(find(endbus==x));
    outnum=b+d;
    if outnum==1
        totalnode(x)=1;
        totalout(x)=1;
        nodecont(x,1)=x;
    elseif outnum==2
        station(linenum+1:linenum+4)=x*ones(4,1);
        stat(linenum+1:linenum+4)=ones(4,1);
        stat(linenum+3)=0;
        startbuscb(linenum+1:linenum+4)=-ones(4,1);
        endbuscb(linenum+1:linenum+4)=-ones(4,1);
        startnode(linenum+1)=x;
        endnode(linenum+1)=nodenum+2;
        startnode(linenum+2)=nodenum+2;
        endnode(linenum+2)=nodenum+1;
        startnode(linenum+3)=x;
        endnode(linenum+3)=nodenum+3;
        startnode(linenum+4)=nodenum+3;
        endnode(linenum+4)=nodenum+1;
        totalnode(x)=4;
        totalout(x)=6;
        nodecont(x,1)=x;
        for y=2:4
            nodecont(x,y)=nodenum+y-1;
        end
        linenum=linenum+4;
        nodenum=nodenum+3;
    end
end

```

```

elseif outnum==3
    station(linenum+1:linenum+5)=x*ones(5,1);
    stat(linenum+1:linenum+5)=ones(5,1);
    stat(linenum+2)=0;
    startbuscb(linenum+1:linenum+5)=-ones(5,1);
    endbuscb(linenum+1:linenum+5)=-ones(5,1);
    startnode(linenum+1)=x;
    endnode(linenum+1)=nodenum+2;
    startnode(linenum+2)=nodenum+2;
    endnode(linenum+2)=nodenum+3;
    startnode(linenum+3)=nodenum+3;
    endnode(linenum+3)=nodenum+1;
    startnode(linenum+4)=x;
    endnode(linenum+4)=nodenum+4;
    startnode(linenum+5)=nodenum+4;
    endnode(linenum+5)=nodenum+1;
    totalnode(x)=5;
    totalout(x)=8;
    nodecont(x,1)=x;
    for y=2:5
        nodecont(x,y)=nodenum+y-1;
    end
    linenum=linenum+5;
    nodenum=nodenum+4;
elseif outnum==4
    station(linenum+1:linenum+6)=x*ones(6,1);
    stat(linenum+1:linenum+6)=ones(6,1);
    stat(linenum+2)=0;
    startbuscb(linenum+1:linenum+6)=-ones(6,1);
    endbuscb(linenum+1:linenum+6)=-ones(6,1);
    startnode(linenum+1)=x;
    endnode(linenum+1)=nodenum+2;
    startnode(linenum+2)=nodenum+2;
    endnode(linenum+2)=nodenum+3;
    startnode(linenum+3)=nodenum+3;
    endnode(linenum+3)=nodenum+1;
    startnode(linenum+4)=x;
    endnode(linenum+4)=nodenum+4;
    startnode(linenum+5)=nodenum+4;
    endnode(linenum+5)=nodenum+5;
    startnode(linenum+6)=nodenum+5;
    endnode(linenum+6)=nodenum+1;
    totalnode(x)=6;
    totalout(x)=10;
    nodecont(x,1)=x;
    for y=2:6
        nodecont(x,y)=nodenum+y-1;
    end
    linenum=linenum+6;
    nodenum=nodenum+5;
elseif outnum==5
    station(linenum+1:linenum+8)=x*ones(8,1);
    stat(linenum+1:linenum+8)=ones(8,1);
    stat(linenum+5)=0;
    stat(linenum+7)=0;

```

```

startbuscb(linenum+1:linenum+8)=-ones(8,1);
endbuscb(linenum+1:linenum+8)=-ones(8,1);
startnode(linenum+1)=x;
endnode(linenum+1)=nodenum+2;
startnode(linenum+2)=nodenum+2;
endnode(linenum+2)=nodenum+3;
startnode(linenum+3)=nodenum+3;
endnode(linenum+3)=nodenum+1;
startnode(linenum+4)=x;
endnode(linenum+4)=nodenum+4;
startnode(linenum+5)=nodenum+4;
endnode(linenum+5)=nodenum+5;
startnode(linenum+6)=nodenum+5;
endnode(linenum+6)=nodenum+1;
startnode(linenum+7)=x;
endnode(linenum+7)=nodenum+6;
startnode(linenum+8)=nodenum+6;
endnode(linenum+8)=nodenum+1;
totalnode(x)=7;
totalout(x)=13;
nodecont(x,1)=x;
for y=2:7
    nodecont(x,y)=nodenum+y-1;
end
linenum=linenum+8;
nodenum=nodenum+6;
elseif outnum==6
    station(linenum+1:linenum+9)=x*ones(9,1);
    stat(linenum+1:linenum+9)=ones(9,1);
    stat(linenum+5)=0;
    stat(linenum+8)=0;
    startbuscb(linenum+1:linenum+9)=-ones(9,1);
    endbuscb(linenum+1:linenum+9)=-ones(9,1);
    startnode(linenum+1)=x;
    endnode(linenum+1)=nodenum+2;
    startnode(linenum+2)=nodenum+2;
    endnode(linenum+2)=nodenum+3;
    startnode(linenum+3)=nodenum+3;
    endnode(linenum+3)=nodenum+1;
    startnode(linenum+4)=x;
    endnode(linenum+4)=nodenum+4;
    startnode(linenum+5)=nodenum+4;
    endnode(linenum+5)=nodenum+5;
    startnode(linenum+6)=nodenum+5;
    endnode(linenum+6)=nodenum+1;
    startnode(linenum+7)=x;
    endnode(linenum+7)=nodenum+6;
    startnode(linenum+8)=nodenum+6;
    endnode(linenum+8)=nodenum+7;
    startnode(linenum+9)=nodenum+7;
    endnode(linenum+9)=nodenum+1;
    totalnode(x)=8;
    totalout(x)=15;
    nodecont(x,1)=x;
    for y=2:8

```

```

        nodecont(x,y)=nodenum+y-1;
    end
    linenum=linenum+9;
    nodenum=nodenum+7;
elseif outnum==7
    station(linenum+1:linenum+11)=x*ones(11,1);
    stat(linenum+1:linenum+11)=ones(11,1);
    stat(linenum+5)=0;
    stat(linenum+8)=0;
    stat(linenum+10)=0;
    startbuscb(linenum+1:linenum+11)=-ones(11,1);
    endbuscb(linenum+1:linenum+11)=-ones(11,1);
    startnode(linenum+1)=x;
    endnode(linenum+1)=nodenum+2;
    startnode(linenum+2)=nodenum+2;
    endnode(linenum+2)=nodenum+3;
    startnode(linenum+3)=nodenum+3;
    endnode(linenum+3)=nodenum+1;
    startnode(linenum+4)=x;
    endnode(linenum+4)=nodenum+4;
    startnode(linenum+5)=nodenum+4;
    endnode(linenum+5)=nodenum+5;
    startnode(linenum+6)=nodenum+5;
    endnode(linenum+6)=nodenum+1;
    startnode(linenum+7)=x;
    endnode(linenum+7)=nodenum+6;
    startnode(linenum+8)=nodenum+6;
    endnode(linenum+8)=nodenum+7;
    startnode(linenum+9)=nodenum+7;
    endnode(linenum+9)=nodenum+1;
    startnode(linenum+10)=x;
    endnode(linenum+10)=nodenum+8;
    startnode(linenum+11)=nodenum+8;
    endnode(linenum+11)=nodenum+1;
    totalnode(x)=9;
    totalout(x)=18;
    nodecont(x,1)=x;
    for y=2:9
        nodecont(x,y)=nodenum+y-1;
    end
    linenum=linenum+11;
    nodenum=nodenum+8;
end
end

sequence=nodecont; % build the detailed node connection for
each branch
for x=1:total_line
    from=startbuscb(x);
    to=endbuscb(x);
    frombus=find(sequence(from,:));
    tobus=find(sequence(to,:));
    if frombus==1
        startnode(x)=sequence(from,1);
    else

```

```

        startnode(x)=sequence(from,frombus(3));
        sequence(from,frombus(3))=0;
    end
    if tobus==1
        endnode(x)=sequence(to,1);
    else
        endnode(x)=sequence(to,tobus(3));
        sequence(to,tobus(3))=0;
    end
end
end

linercb=zeros(linenum,1);
linexcb=zeros(linenum,1);
supcb=zeros(linenum,1);
concb=zeros(linenum,1);
linercb(1:total_line)=liner';
linexcb(1:total_line)=linex';
supcb(1:total_line)=sup';
concb(1:total_line)=con';

pflownum=0;

for x=1:total_bus
    z=1;
    for y=1:total_pflow
        measurements for the non-zero impedacne branches
        if startbuspflow(y)==x
            lnum=linenum+pflow(y);
            linenum+pflowcb(pflownum+z)=lnum;
            if startbuscb(lnum)==x
                startbuspflowcb(pflownum+z)=startnode(lnum);
                endbuspflowcb(pflownum+z)=endnode(lnum);
            else
                startbuspflowcb(pflownum+z)=endnode(lnum);
                endbuspflowcb(pflownum+z)=startnode(lnum);
            end
            end
            measurepflowcb(pflownum+z)=measurepflow(y);
            measureweightpflowcb(pflownum+z)=measureweightpflow(y);
            z=z+1;
        end
    end
    if totalnode(x)==1
        measurements for CB in each substation
        measnum=1;
        stationpflow(pflownum+1)=x;
        pflownum=pflownum+1;
    elseif totalnode(x)==4
        measnum=5;
        stationpflow(pflownum+1:pflownum+5)=x*ones(5,1);
        for y=1:total_pinj
            if buspinj(y)==x
                pinj=measurepinj(y);
            end
        end
        end
        david=linenum+pflowcb(pflownum+1:pflownum+2);
    end
end

```

```

for z=1:2
    [C,I]=min(david);
    pflow(z)=measurepflowcb(pflownum+I);
    david(I)=9999;
end
for y=1:linenum
    if station(y)==x && stat(y)==1
        linenumflowcb(pflownum+3)=y;
        startbuspflowcb(pflownum+3)=startnode(y);
        endbuspflowcb(pflownum+3)=endnode(y);
        measurepflowcb(pflownum+3)=pinj;
        measureweightpflowcb(pflownum+3)=1e-6;
        break;
    end
end
linenumflowcb(pflownum+4)=y+1;
startbuspflowcb(pflownum+4)=startnode(y+1);
endbuspflowcb(pflownum+4)=endnode(y+1);
measurepflowcb(pflownum+4)=pinj-pflow(1);
measureweightpflowcb(pflownum+4)=1e-6;
linenumflowcb(pflownum+5)=y+3;
startbuspflowcb(pflownum+5)=startnode(y+3);
endbuspflowcb(pflownum+5)=endnode(y+3);
measurepflowcb(pflownum+5)=-pflow(2);
measureweightpflowcb(pflownum+5)=1e-6;
pflownum=pflownum+5;
elseif totalnode(x)==5
    measnum=7;
    stationpflow(pflownum+1:pflownum+7)=x*ones(7,1);
    for y=1:total_pinj
        if buspinj(y)==x
            pinj=measurepinj(y);
        end
    end
end
david=linenumflowcb(pflownum+1:pflownum+3);
for z=1:3
    [C,I]=min(david);
    pflow(z)=measurepflowcb(pflownum+I);
    david(I)=9999;
end
for y=1:linenum
    if station(y)==x && stat(y)==1
        linenumflowcb(pflownum+4)=y;
        startbuspflowcb(pflownum+4)=startnode(y);
        endbuspflowcb(pflownum+4)=endnode(y);
        measurepflowcb(pflownum+4)=pflow(1);
        measureweightpflowcb(pflownum+4)=1e-6;
        break;
    end
end
linenumflowcb(pflownum+5)=y+2;
startbuspflowcb(pflownum+5)=startnode(y+2);
endbuspflowcb(pflownum+5)=endnode(y+2);
measurepflowcb(pflownum+5)=-pflow(2);
measureweightpflowcb(pflownum+5)=1e-6;

```

```

linenumpflowcb(pflownum+6)=y+3;
startbuspflowcb(pflownum+6)=startnode(y+3);
endbuspflowcb(pflownum+6)=endnode(y+3);
measurepflowcb(pflownum+6)=pinj-pflow(1);
measureweightpflowcb(pflownum+6)=1e-6;
linenumpflowcb(pflownum+7)=y+4;
startbuspflowcb(pflownum+7)=startnode(y+4);
endbuspflowcb(pflownum+7)=endnode(y+4);
measurepflowcb(pflownum+7)=pflow(2);
measureweightpflowcb(pflownum+7)=1e-6;
pflownum=pflownum+7;
elseif totalnode(x)==6
measnum=9;
stationpflow(pflownum+1:pflownum+9)=x*ones(9,1);
for y=1:total_pinj
    if buspinj(y)==x
        pinj=measurepinj(y);
    end
end
david=linenumpflowcb(pflownum+1:pflownum+4);
for z=1:4
    [C,I]=min(david);
    pflow(z)=measurepflowcb(pflownum+I);
    david(I)=9999;
end
for y=1:linenum
    if station(y)==x && stat(y)==1
        linenumpflowcb(pflownum+5)=y;
        startbuspflowcb(pflownum+5)=startnode(y);
        endbuspflowcb(pflownum+5)=endnode(y);
        measurepflowcb(pflownum+5)=pflow(1);
        measureweightpflowcb(pflownum+5)=1e-6;
        break;
    end
end
linenumpflowcb(pflownum+6)=y+2;
startbuspflowcb(pflownum+6)=startnode(y+2);
endbuspflowcb(pflownum+6)=endnode(y+2);
measurepflowcb(pflownum+6)=-pflow(2);
measureweightpflowcb(pflownum+6)=1e-6;
linenumpflowcb(pflownum+7)=y+3;
startbuspflowcb(pflownum+7)=startnode(y+3);
endbuspflowcb(pflownum+7)=endnode(y+3);
measurepflowcb(pflownum+7)=pinj-pflow(1);
measureweightpflowcb(pflownum+7)=1e-6;
linenumpflowcb(pflownum+8)=y+4;
startbuspflowcb(pflownum+8)=startnode(y+4);
endbuspflowcb(pflownum+8)=endnode(y+4);
measurepflowcb(pflownum+8)=pflow(2)+pflow(4);
measureweightpflowcb(pflownum+8)=1e-6;
linenumpflowcb(pflownum+9)=y+5;
startbuspflowcb(pflownum+9)=startnode(y+5);
endbuspflowcb(pflownum+9)=endnode(y+5);
measurepflowcb(pflownum+9)=pflow(2);
measureweightpflowcb(pflownum+9)=1e-6;

```

```

    pflownum=pflownum+9;
elseif totalnode(x)==7
    measnum=11;
    stationpflow(pflownum+1:pflownum+11)=x*ones(11,1);
    for y=1:total_pinj
        if buspinj(y)==x
            pinj=measurepinj(y);
        end
    end
    david=linenumpflowcb(pflownum+1:pflownum+5);
    for z=1:5
        [C,I]=min(david);
        pflow(z)=measurepflowcb(pflownum+I);
        david(I)=9999;
    end
    end
    for y=1:linenum
        if station(y)==x && stat(y)==1
            linenumpflowcb(pflownum+6)=y;
            startbuspflowcb(pflownum+6)=startnode(y);
            endbuspflowcb(pflownum+6)=endnode(y);
            measurepflowcb(pflownum+6)=pinj-pflow(3);
            measureweightpflowcb(pflownum+6)=1e-6;
            break;
        end
    end
    linenumpflowcb(pflownum+7)=y+1;
    startbuspflowcb(pflownum+7)=startnode(y+1);
    endbuspflowcb(pflownum+7)=endnode(y+1);
    measurepflowcb(pflownum+7)=pinj-pflow(3)-pflow(1);
    measureweightpflowcb(pflownum+7)=1e-6;
    linenumpflowcb(pflownum+8)=y+2;
    startbuspflowcb(pflownum+8)=startnode(y+2);
    endbuspflowcb(pflownum+8)=endnode(y+2);
    measurepflowcb(pflownum+8)=pflow(4)+pflow(5);
    measureweightpflowcb(pflownum+8)=1e-6;
    linenumpflowcb(pflownum+9)=y+3;
    startbuspflowcb(pflownum+9)=startnode(y+3);
    endbuspflowcb(pflownum+9)=endnode(y+3);
    measurepflowcb(pflownum+9)=pflow(3);
    measureweightpflowcb(pflownum+9)=1e-6;
    linenumpflowcb(pflownum+10)=y+5;
    startbuspflowcb(pflownum+10)=startnode(y+5);
    endbuspflowcb(pflownum+10)=endnode(y+5);
    measurepflowcb(pflownum+10)=-pflow(4);
    measureweightpflowcb(pflownum+10)=1e-6;
    linenumpflowcb(pflownum+11)=y+7;
    startbuspflowcb(pflownum+11)=startnode(y+7);
    endbuspflowcb(pflownum+11)=endnode(y+7);
    measurepflowcb(pflownum+11)=-pflow(5);
    measureweightpflowcb(pflownum+11)=1e-6;
    pflownum=pflownum+11;
elseif totalnode(x)==8
    measnum=12;
    stationpflow(pflownum+1:pflownum+13)=x*ones(13,1);
    for y=1:total_pinj

```

```

        if buspinj(y)==x
            pinj=measurepinj(y);
        end
    end
    david=linenumpflowcb(pflownum+1:pflownum+6);
    for z=1:6
        [C,I]=min(david);
        pflow(z)=measurepflowcb(pflownum+I);
        david(I)=9999;
    end
    for y=1:linenum
        if station(y)==x && stat(y)==1
            linenumpflowcb(pflownum+7)=y;
            startbuspflowcb(pflownum+7)=startnode(y);
            endbuspflowcb(pflownum+7)=endnode(y);
            measurepflowcb(pflownum+7)=pinj-pflow(3)-pflow(5);
            measureweightpflowcb(pflownum+7)=1e-6;
            break;
        end
    end
    linenumpflowcb(pflownum+8)=y+1;
    startbuspflowcb(pflownum+8)=startnode(y+1);
    endbuspflowcb(pflownum+8)=endnode(y+1);
    measurepflowcb(pflownum+8)=pinj-pflow(3)-pflow(5)-pflow(1);
    measureweightpflowcb(pflownum+8)=1e-6;
    linenumpflowcb(pflownum+9)=y+2;
    startbuspflowcb(pflownum+9)=startnode(y+2);
    endbuspflowcb(pflownum+9)=endnode(y+2);
    measurepflowcb(pflownum+9)=pflow(4)+pflow(6);
    measureweightpflowcb(pflownum+9)=1e-6;
    linenumpflowcb(pflownum+10)=y+3;
    startbuspflowcb(pflownum+10)=startnode(y+3);
    endbuspflowcb(pflownum+10)=endnode(y+3);
    measurepflowcb(pflownum+10)=pflow(3);
    measureweightpflowcb(pflownum+10)=1e-6;
    linenumpflowcb(pflownum+11)=y+5;
    startbuspflowcb(pflownum+11)=startnode(y+5);
    endbuspflowcb(pflownum+11)=endnode(y+5);
    measurepflowcb(pflownum+11)=-pflow(4);
    measureweightpflowcb(pflownum+11)=1e-6;
    linenumpflowcb(pflownum+12)=y+6;
    startbuspflowcb(pflownum+12)=startnode(y+6);
    endbuspflowcb(pflownum+12)=endnode(y+6);
    measurepflowcb(pflownum+12)=pflow(5);
    measureweightpflowcb(pflownum+12)=1e-6;
    linenumpflowcb(pflownum+13)=y+8;
    startbuspflowcb(pflownum+13)=startnode(y+8);
    endbuspflowcb(pflownum+13)=endnode(y+8);
    measurepflowcb(pflownum+13)=-pflow(6);
    measureweightpflowcb(pflownum+13)=1e-6;
    pflownum=pflownum+13;
elseif totalnode(x)==9
    measnum=15;
    stationpflow(pflownum+1:pflownum+15)=x*ones(15,1);
    for y=1:total_pinj

```

```

        if buspinj(y)==x
            pinj=measurepinj(y);
        end
    end
david=linenumpflowcb(pflownum+1:pflownum+7);
for z=1:7
    [C,I]=min(david);
    pflow(z)=measurepflowcb(pflownum+I);
    david(I)=9999;
end
for y=1:linenum
    if station(y)==x && stat(y)==1
        linenumpflowcb(pflownum+8)=y;
        startbuspflowcb(pflownum+8)=startnode(y);
        endbuspflowcb(pflownum+8)=endnode(y);
        measurepflowcb(pflownum+8)=pinj-pflow(3)-pflow(5);
        measureweightpflowcb(pflownum+8)=1e-6;
        break;
    end
end
linenumpflowcb(pflownum+9)=y+1;
startbuspflowcb(pflownum+9)=startnode(y+1);
endbuspflowcb(pflownum+9)=endnode(y+1);
measurepflowcb(pflownum+9)=pinj-pflow(3)-pflow(5)-pflow(1);
measureweightpflowcb(pflownum+9)=1e-6;
linenumpflowcb(pflownum+10)=y+2;
startbuspflowcb(pflownum+10)=startnode(y+2);
endbuspflowcb(pflownum+10)=endnode(y+2);
measurepflowcb(pflownum+10)=pflow(4)+pflow(6)+pflow(7);
measureweightpflowcb(pflownum+10)=1e-6;
linenumpflowcb(pflownum+11)=y+3;
startbuspflowcb(pflownum+11)=startnode(y+3);
endbuspflowcb(pflownum+11)=endnode(y+3);
measurepflowcb(pflownum+11)=pflow(3);
measureweightpflowcb(pflownum+11)=1e-6;
linenumpflowcb(pflownum+12)=y+5;
startbuspflowcb(pflownum+12)=startnode(y+5);
endbuspflowcb(pflownum+12)=endnode(y+5);
measurepflowcb(pflownum+12)=-pflow(4);
measureweightpflowcb(pflownum+12)=1e-6;
linenumpflowcb(pflownum+13)=y+6;
startbuspflowcb(pflownum+13)=startnode(y+6);
endbuspflowcb(pflownum+13)=endnode(y+6);
measurepflowcb(pflownum+13)=pflow(5);
measureweightpflowcb(pflownum+13)=1e-6;
linenumpflowcb(pflownum+14)=y+8;
startbuspflowcb(pflownum+14)=startnode(y+8);
endbuspflowcb(pflownum+14)=endnode(y+8);
measurepflowcb(pflownum+14)=-pflow(6);
measureweightpflowcb(pflownum+14)=1e-6;
linenumpflowcb(pflownum+15)=y+10;
startbuspflowcb(pflownum+15)=startnode(y+10);
endbuspflowcb(pflownum+15)=endnode(y+10);
measurepflowcb(pflownum+15)=-pflow(7);
measureweightpflowcb(pflownum+15)=1e-6;

```

```

        pflownum=pflownum+15;
    end
end

% Output the results

foutput = fopen('topoanainput.dat','w');

for x=1:total_bus
    fprintf(foutput, '%d%5d%5d',x,totalnode(x),totalout(x));
    for y=1:totalnode(x)
        fprintf(foutput, '%5d',nodecont(x,y));
    end
    fprintf(foutput, '\n');
end
fprintf(foutput, '%d',-99);

for x=1:linenum
    if x<=total_line

fprintf(foutput, '\n%d%5d%5d%5d%6.3f%5d%5d%5d%5d%10.5f%12.5f%12.5f%12.5f',x
,station(x),stat(x),linetype(x),linetap(x),startbuscb(x),endbuscb(x),start
node(x),endnode(x),linercb(x),linexcb(x),concb(x),supcb(x));
        else

fprintf(foutput, '\n%d%5d%5d%5d%6d%5d%5d%5d%10.5f%12.5f%12.5f%12.5f',x,s
tation(x),stat(x),-1,-
1,startbuscb(x),endbuscb(x),startnode(x),endnode(x),linercb(x),linexcb(x),
concb(x),supcb(x));
        end
    end
    fprintf(foutput, '\n%d',-99);

    fprintf(foutput, '\n\n');
    fclose(foutput);

    foutput = fopen('topomeasure.dat','w');

    for x=1:pflownum

        fprintf(foutput, '%d%5d%5d%5d%5d%12.6f%12.6f\n',1,stationpflow(x),linenumpf
lowcb(x),startbuspflowcb(x),endbuspflowcb(x),measurepflowcb(x),measureweig
htpflowcb(x));
        end
        fprintf(foutput, '%d\n',-99);

        [b,busseq]=sort(buspinj);

        for x=1:total_pinj
            y=busseq(x);

            fprintf(foutput, '%d%5d%5d%12.6f%12.6f\n',3,x,x,measurepinj(y),measureweigh
tpinj(y));
            end
            fprintf(foutput, '%d\n',-99);
        end
    end
end

```

```
fprintf(foutput, '\n\n');  
fclose(foutput);
```